

***Insights into Binder
Chemistry, Microstructure,
Properties Relationships
-
Usage in the Real World***

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June 1-5, 2014

Raleigh, North Carolina, USA

WesternResearch
I N S T I T U T E

- **Background - Context**
- **Chemical-physical and structural properties of asphalt**
 - **Impact on asphalt mechanical properties**
- **Asphalt modification**
 - **Impact on structure and mechanical properties**
- **Summary**
- **Perspectives**



- **Asphalt binders behavior dependency**
 - Crude oil origin and process
 - Temperature and time dependency of molecular interactions and asphalt structure
 - Aging impact
 - Chemical Oxidation – Plant and in-service aging
 - Physical aging – testing and in-service
 - Additives chemistry / physical properties and their interactions / compatibility with asphalt
- **Importance of understanding the relationships between composition–structure-properties**
 - Refiner / asphalt binder-additive supplier: crude selection / binder formulation and process
 - Applicator / contractor: mix design and application
 - Owner: specification and pavement performance



- **A challenge**
 - *So much knowledge acquired, worldwide*
 - *But so much unknown, still!...*
- **Focus**
 - **Some particular aspects of asphalt structure – influence of additives**
 - **Examples of some innovative binder characterization methods**
 - **Meaning of the results in the real world – testing and performance**
 - **Not meant to be exhaustive, but to reconnect some dots**
- **A long trip through history, present time and... the future?**
 - **My deepest acknowledgements to fine researchers / technologists:**
 - Anderson, Bahia, Brule, Claudy, D'Angelo, Di Benedetto, Jones, King, Kluttz, Lapalu, Lesueur, Letoffe, Little, Mouillet, Schabron. Pauli, Petersen, Redelius, Rowe, Such, Turner, Youtcheff, ...
 - WRI, TU Delft, Nottingham, ENTPE, KTH, IFFSTAR (LCPC), FHWA, and BP, Kraton Polymers, Nynas, Shell, Total (Elf)...

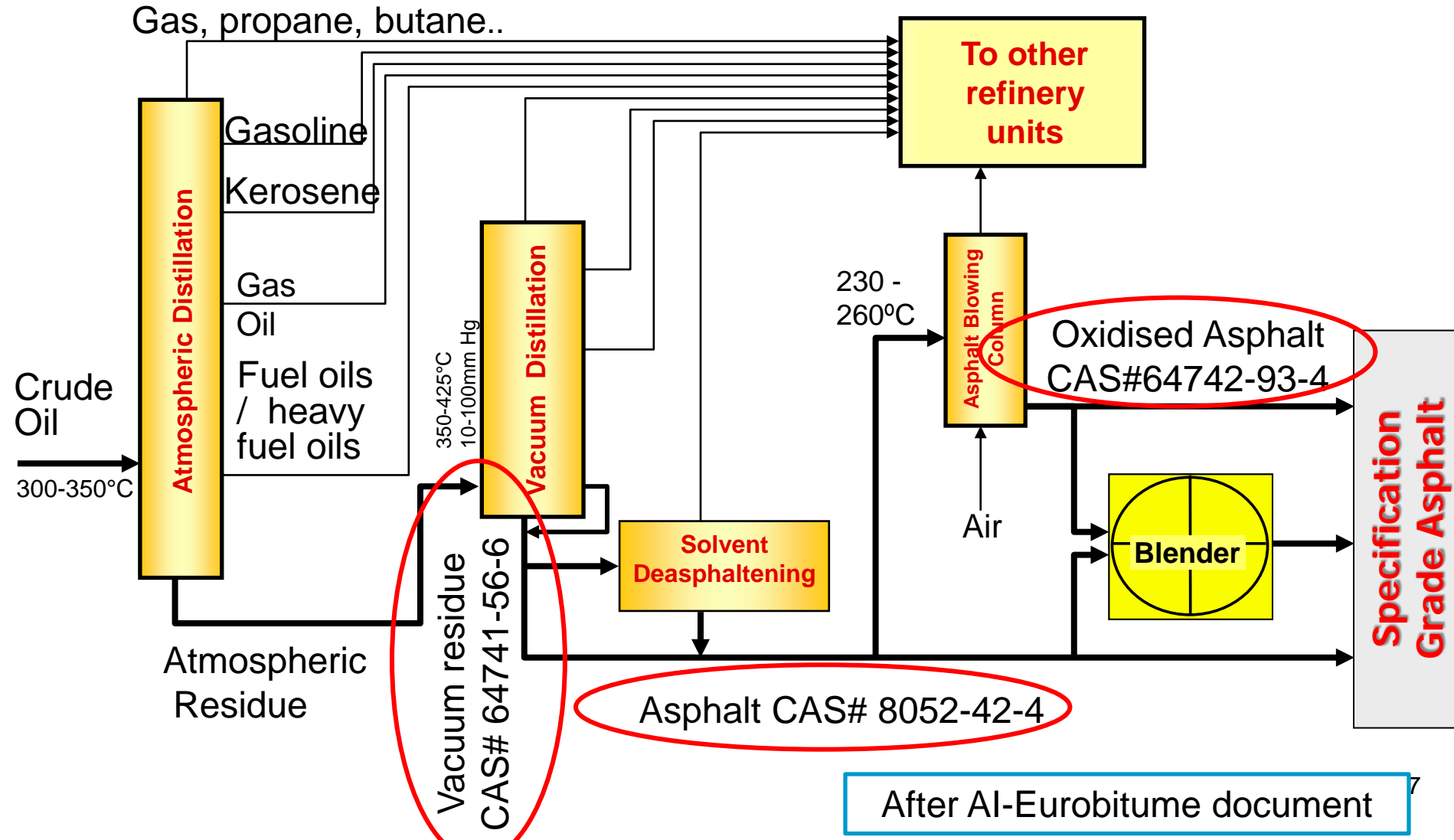
- **Background - Context**
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- **Asphalt = a blend of complex hydrocarbons**
 - Viscous and black
 - **Complex composition = the chemistry supermarket!**
 - Ten-Hundred Thousands of different molecules
 - Polarity and aromatic continuum
 - Associated species
- **Elemental composition**

• Carbon	83-87%
• Hydrogen	10-14%
• Heteroatoms: Sulfur, Oxygen, Nitrogen	1-9%
• Vanadium, Nickel, Iron	1-2000 ppm
- **Specificities**
 - Hydrogen deficient hydrocarbons
 - Ni/V and C/H sometimes used as crude oil or process tracers

Refinery Block Diagram



After AI-Eurobitume document

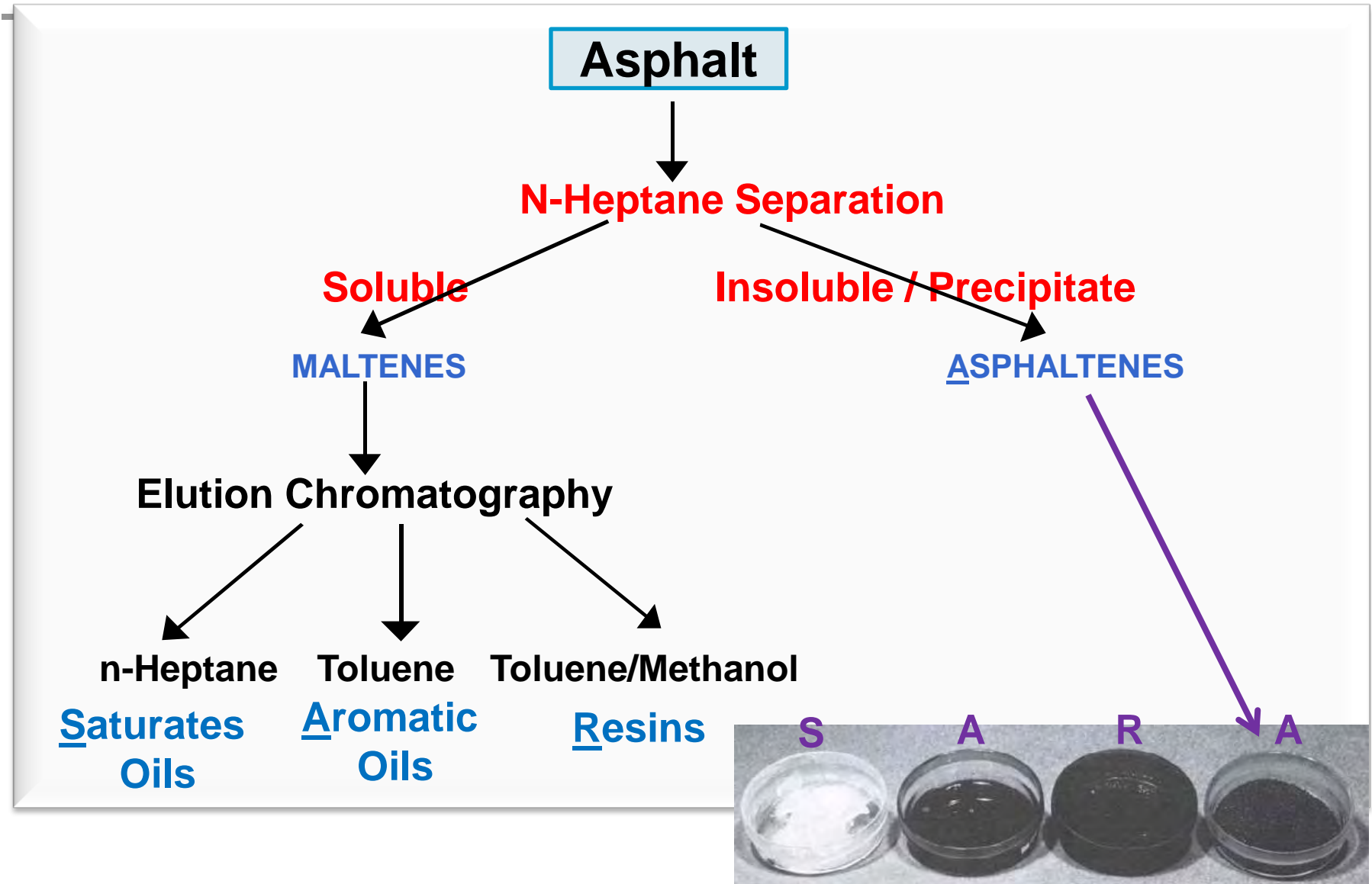
•Complex Asphalt production process (Europe-US)

- Examples from the SHRP AMRL library

MRL Code	AAA-1	AAA-2	AAB-1	AAB-2	AAC-1	AAC-2	AAD-1
Crude Oil Source	Lloydminster		WY Sour		Redwater		Ca Coast
Elemental Analysis							
C, %	83.9	84.12	82.3	85.7	86.5	86.6	81.6
H, %	10.0	10.59	10.6	10.59	11.3	10.6	10.8
O, %	0.6		0.8		0.9	1.0	0.9
Nitrogen, %	0.50	0.50	0.54	0.54	0.66	0.90	0.77
Sulfur, %	5.50	6.00	4.70	5.40	1.90	1.90	6.90
Vanadium, ppm	174	138	220	163	146	100	310
Nickel, ppm	86	77	56	36	63	55	145
Fe, ppm	<1		16			29	13

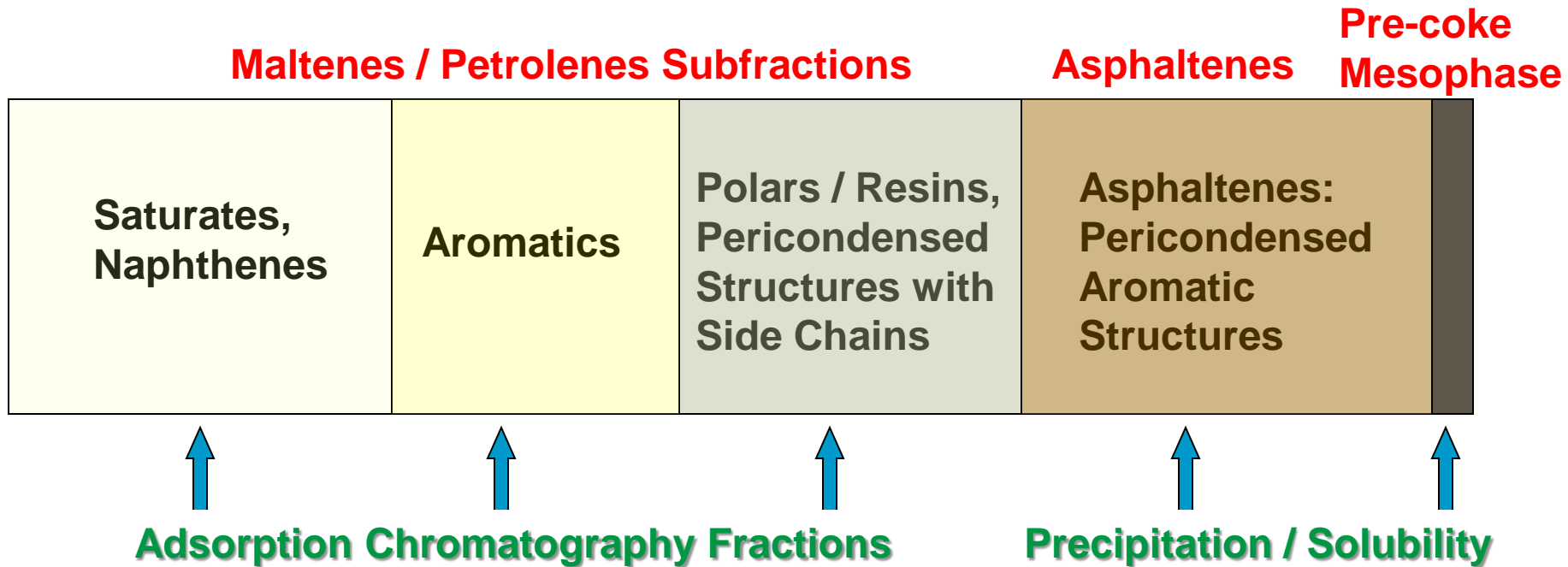
- Dependence on crude oil origin & process
 - Only 10% all crude oils yield asphalt!
- Generic fraction composition to overcome the complexity

Generic fractions of Asphalt



Generic fractions of Asphalt

- Asphalt SARA separation in fractions of a continuum
- Fraction chemistry defined by the particular methods and/or solvents used



Generic fractions of Asphalt

- Asphaltenes are also part of the continuum
- Asphaltene subfractions can also be defined / separated according to their solubility in solvents

Resins-like	More Aromatic	Fewer Alkyl Side Chains	Pre-Coke
Heptane	Cyclohexane	Toluene	CH ₂ Cl ₂ : MeOH

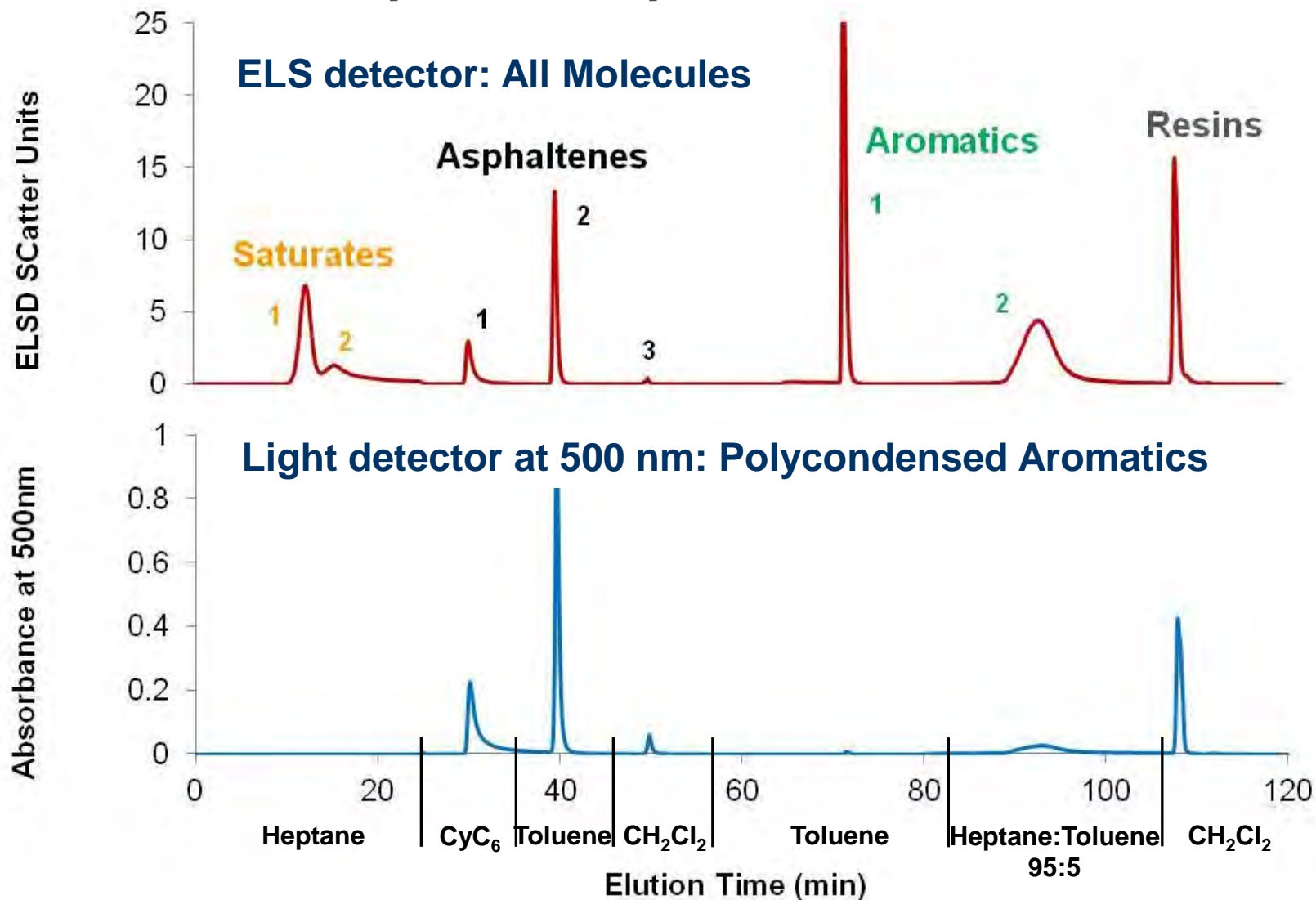


Aromaticity and Polarity Increase

- Some of the fractions consist of associated species

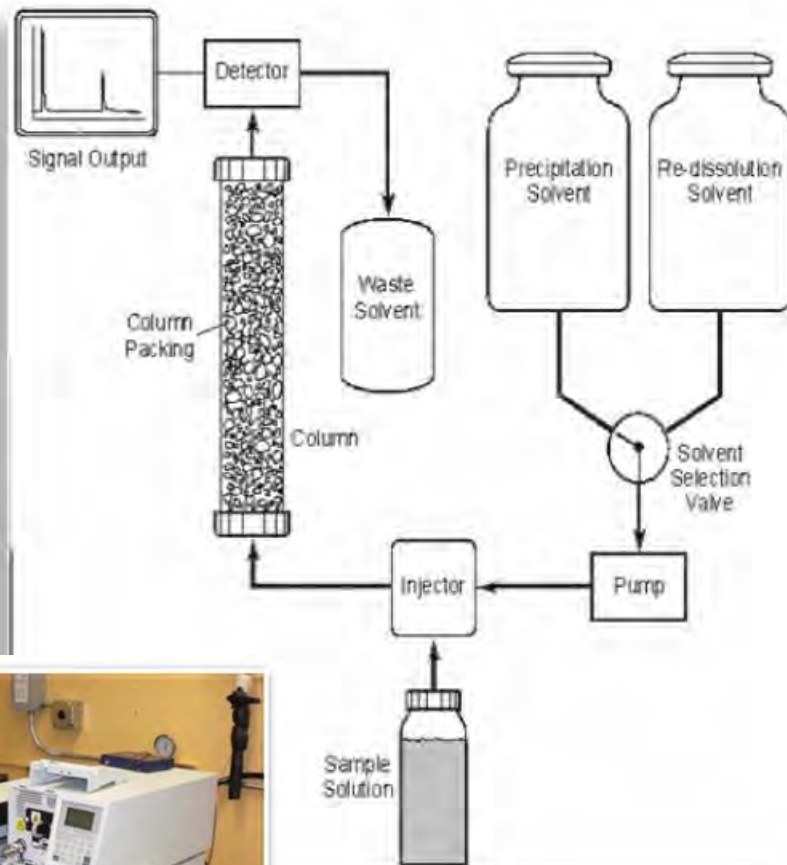
Generic fractions of asphalt

- **SAR-AD™** separates asphalt into 8 fractions



- Asphalts & Heavy Oils separation by SAR-AD™
- Rapid & Relevant analytical tool developed by WRI

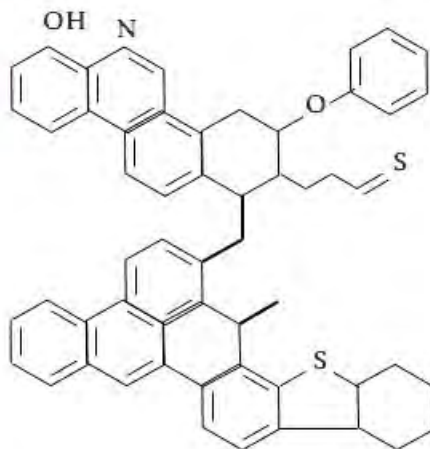
- Whole product injected (2 mg) separated in 4hrs
- 4 separation columns
 - Maltenes & varnish
 - Polars/resins
 - Saturates and aromatics
 - Asphaltene subfractions
- Dual detection by ELSD and Light
- Repeated injections



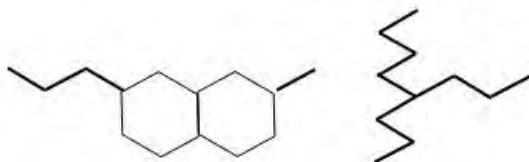
SAR-AD™ patented

Asphalt generic fractions Model molecules and structures

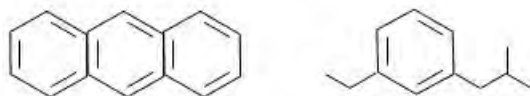
Asphaltenes



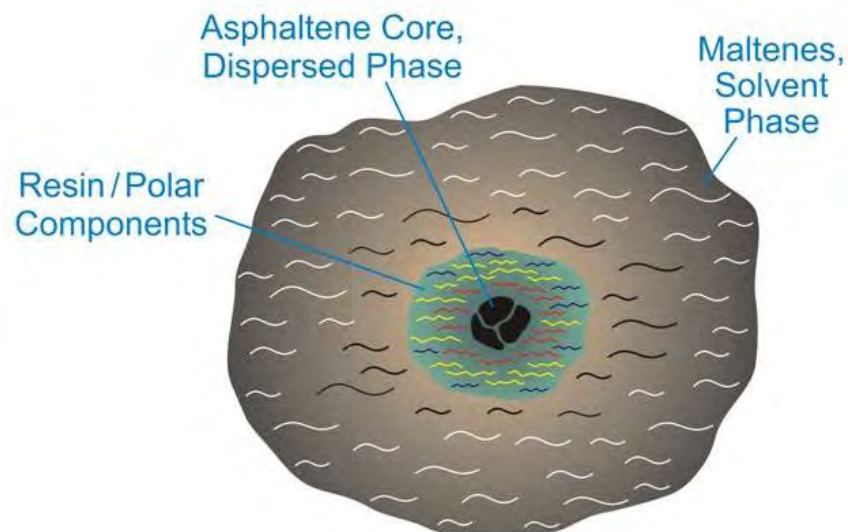
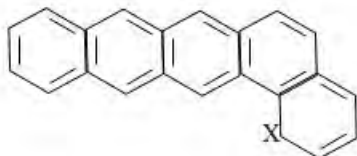
Saturates



Aromatics



Resins

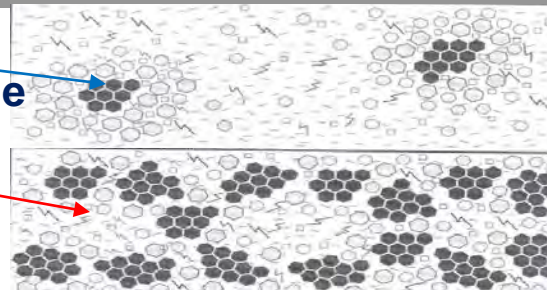
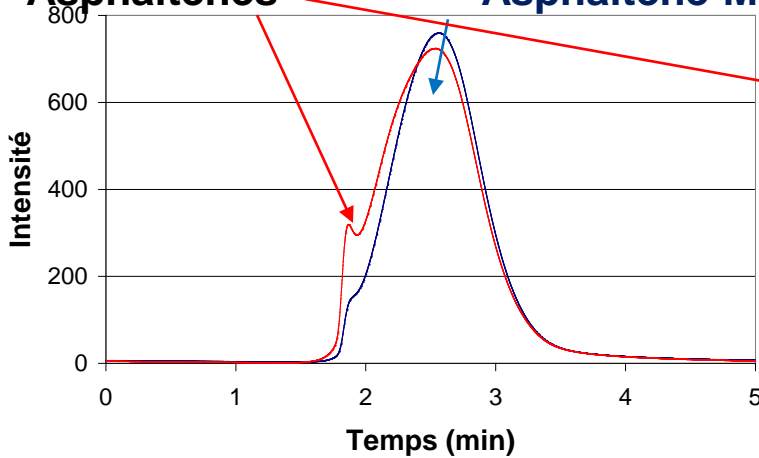


**Asphalt Colloidal
structure model**

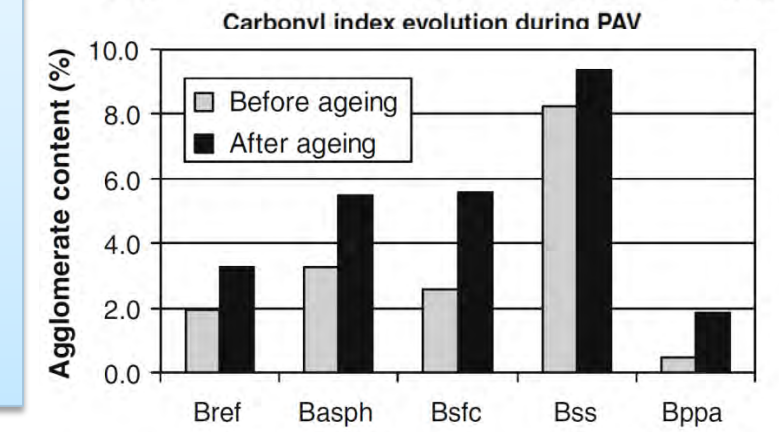
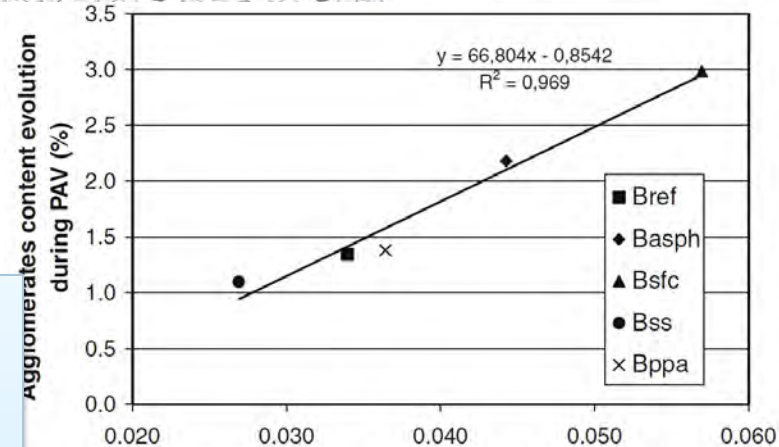
- **Hypothesis: Asphalt molecules assembly in a colloidal structure – temperature dependent**
- **SOL = Asphaltene micelles well «peptized» / dispersed in the maltene “solvent” matrix**
 - Low content in asphaltenes and saturates
 - High content in aromatics and resins
- **GEL = Asphaltene micelles poorly « peptized »**
 - High content in asphaltenes and saturates
 - Low content in aromatics and resins
- **At high temperature: homogeneous SOL structure**
 - Brownian relaxation above about 80C where interactions, polar, H-Bonds... in asphaltenes and resins are destroyed
- **Boussingault (1837), Nellensteyn (1923), Pfeiffer (1940), Yen, Storm, Pal-Rhodes, Lesueur (1996),... revisited**

Agglomerated Asphaltenes

Dispersed Asphaltene Micelle



**SOL/GEL
Shell Model**



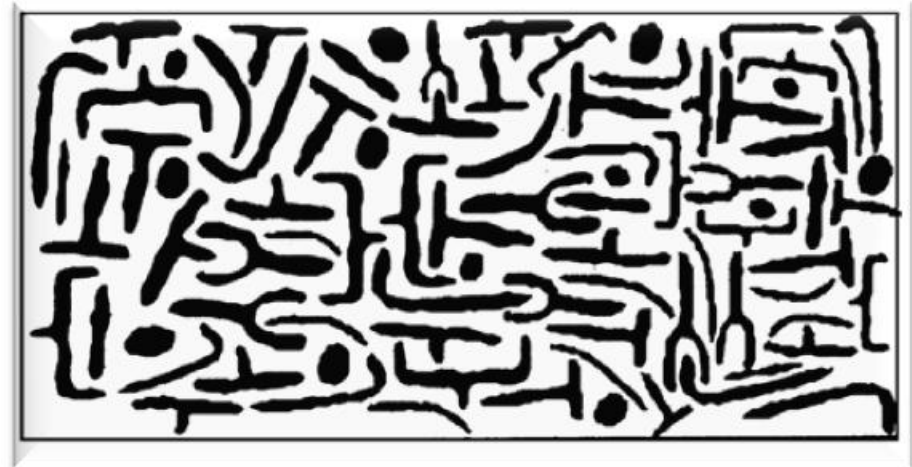
•Sol-Gel asphaltene molecular association (peak) evaluated by High speed SEC

- Increase during aging - Correlated with carbonyl and sulfoxide formation
- Asphalt source, additive and process dependant
- Works: *Brule, Such (80's), Jennings, Pribanic (90's), Chailleux, Mouillet (2010's)*

- Developed under SHRP - based on fluid polarity
- **Asphalts: homogeneous concentrated mixtures of polar materials dispersed in neutral materials**
 - Polars in a continuous, rather homogeneous, 3-D network
 - No asphaltene but a range of polar compounds - strong/weak acid/bases through amphoteric
 - Oxidation effect: molecular species sensitive to oxidation, increase the polar content, the size and strength of the 3-D microstructure

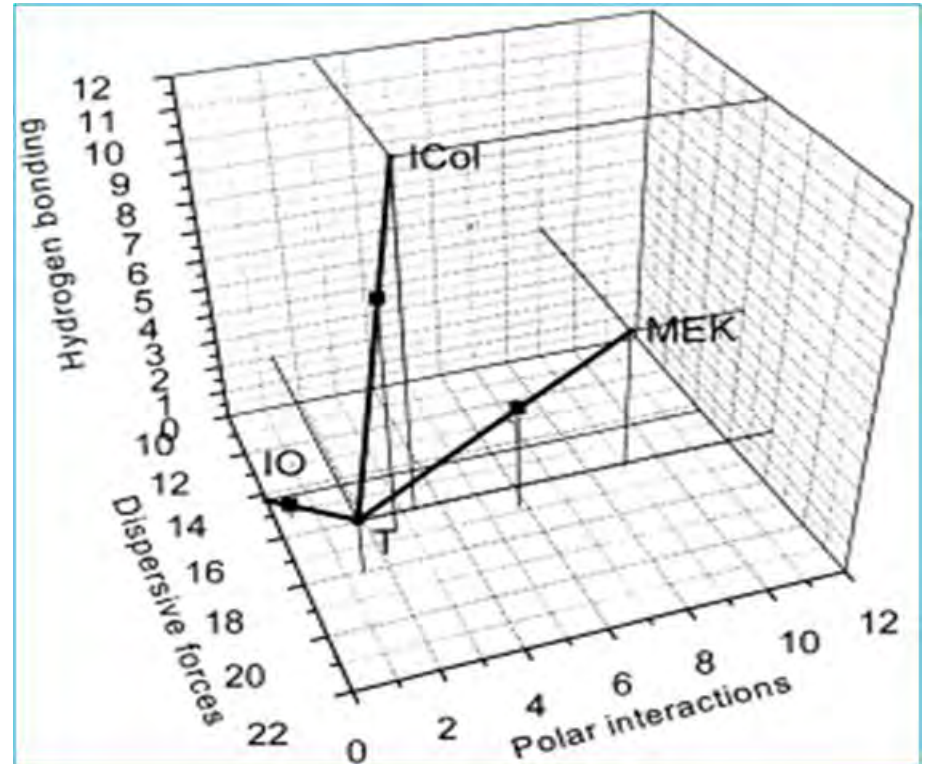
After:

- Robertson et al
- Jones et al



3D Solubility parameter

- Accounts for various interactions between the various bitumen molecules
 - H-Bond
 - Polar
 - Wan der waals
- Dedicated to embrace solubility issues as a whole



Black Squares = Precipitation Points

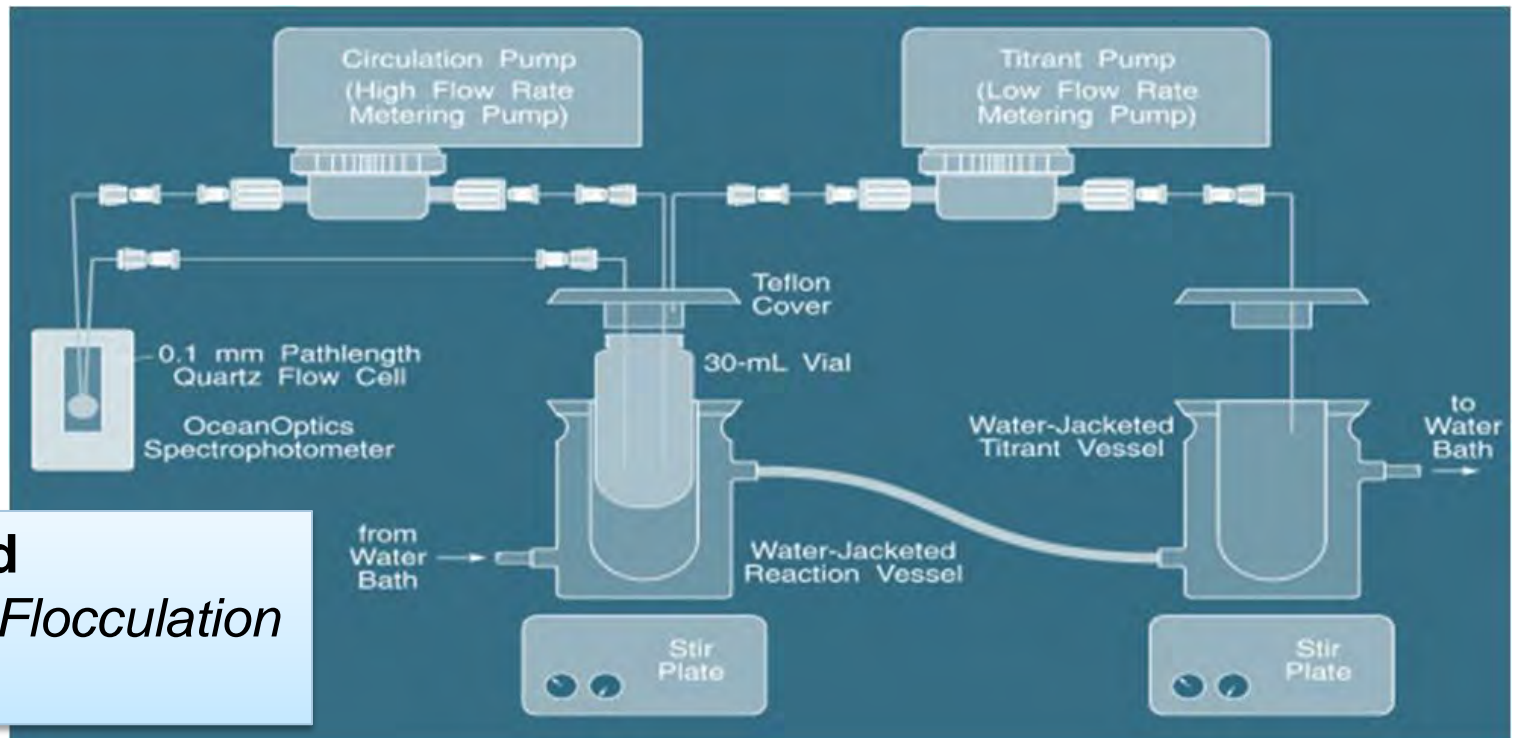
Diagram of Titration of Venezuelan Bitumen

By Redelius - Credit To Fuel 79 (2000) 18

- **Compatibility concept - “Operational”**
 - **Mixing similar materials gives expected results - linear rule - blending**
 - **Consequently incompatibility is when mixing similar materials gives unexpected results - non-linear - like softer or stiffer than expected**
 - **Ex: mixing incompatible asphaltenes from different asphalts (study from Anderson, Petersen)**

Mix #	Components of Mixture	Neat			TFOT + PAV, 60°C, 144 hours		
		Vis., Pa•s 25°C, 1 r/s	Tan δ 5°C, 1 r/s	R. S. Visc. 25°C, 1 r/s	Vis., Pa•s 25°C, 1 r/s	Tan δ 25°C, 1 r/s	Aging Index 60°C, 1 r/s
I (A)	AAD Maltenes (79%) AAD Asphaltenes (21%)	49,011	3.2	705	550,650	1.5	15.4
VII (B)	AAG Maltenes (94%) AAG Asphaltenes (6%)	389,100	6.3	64	1,086,400	1.6	4.2
Cross Blends							
V (C)	AAG Maltenes (79%) AAD Asphaltenes (21%)	4,970,900	1.5	287 (?)*	20,662,000	0.8	15.5
III (A) (C)	AAD Maltenes (79%) AAG Asphaltenes (21%)	62,908	3.7	906	552,310	1.8	9.0

- **Compatibility: function of the maltene solvent power and the asphaltene dispersion (ref. Heithaus)**
 - Measured by Asphaltene Flocculation Titration
 - P_a and P_o peptizability of the asphaltenes and maltenes
 - P-value: state of peptization of the Asphalt (or the oil)



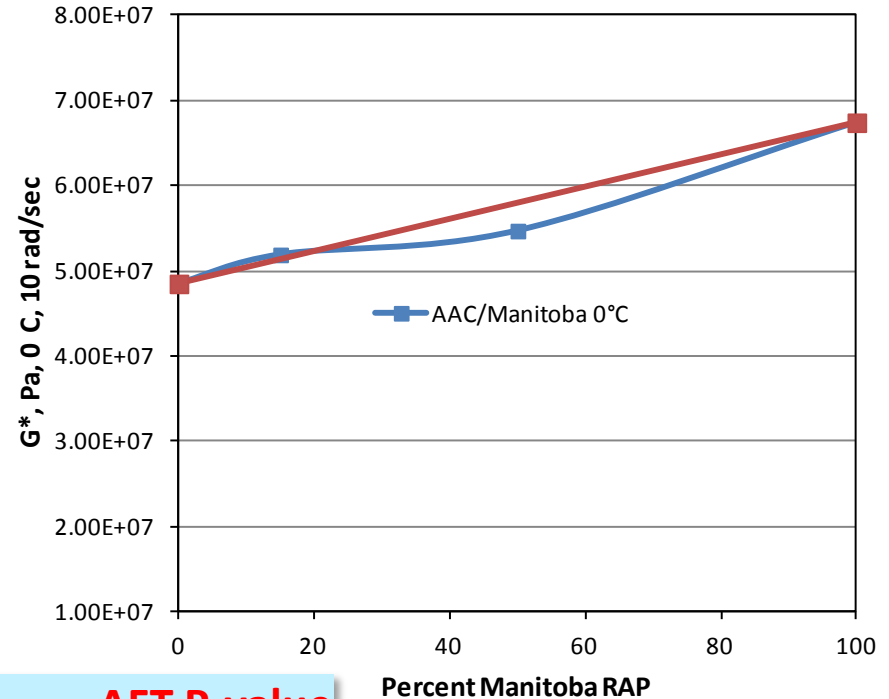
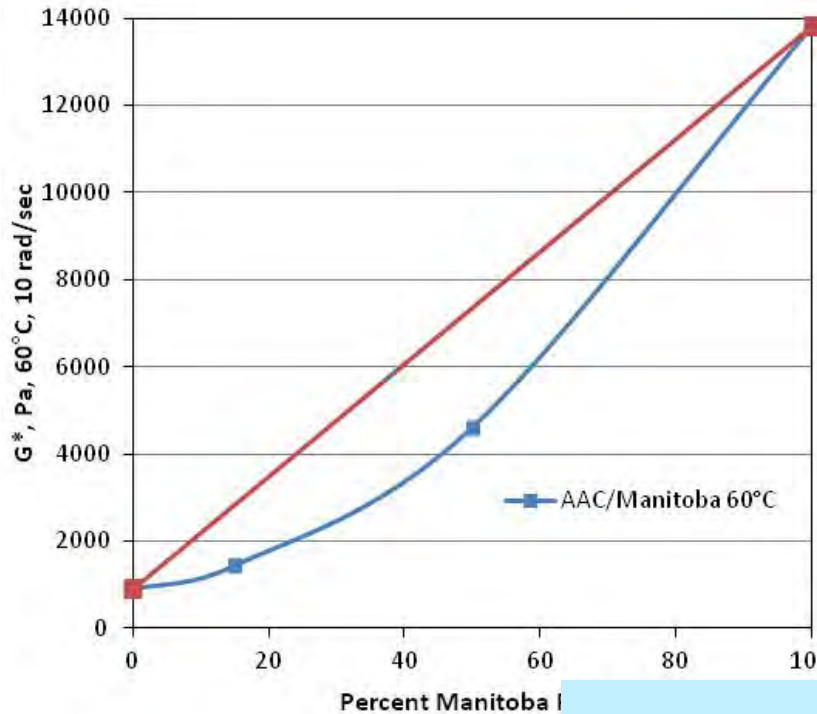
WRI method

*Automated Flocculation
Titrimeter®*

- **Colloidal structure parameters from SAR-AD, AFT, DSC and SEC can / could be used to assess compatibility, blending rules and aging effects**
 - Blends of various asphalt bases available in refineries
 - Virgin asphalt and RAP or RAS blends
 - Polymers / additives for asphalt modification
 - Binder oxidative and physical aging
 - No standard to identify the borderline between “compatible” and “incompatible” asphalt
- **Example 1 - compatibility of SBS PMBs assessed using the instability index**
 - Gaestel index $I_c = (\text{Saturates} + \text{Asphaltenes}) / (\text{Aromatics} + \text{Resins})$
 - When I_c increases, the colloidal stability decreases
 - Rule of thumb: the lower the I_c (higher aromatics), the more compatible the SBS-Asphalt system (after Airey UNOTT, Brule LCPC,...)

Example 2: Virgin binder + RAP – lab blends

- AAC-1 – Manitoba RAP / G^* measured at 60 and 0C / 10 rad/sec



Unpredictable blend

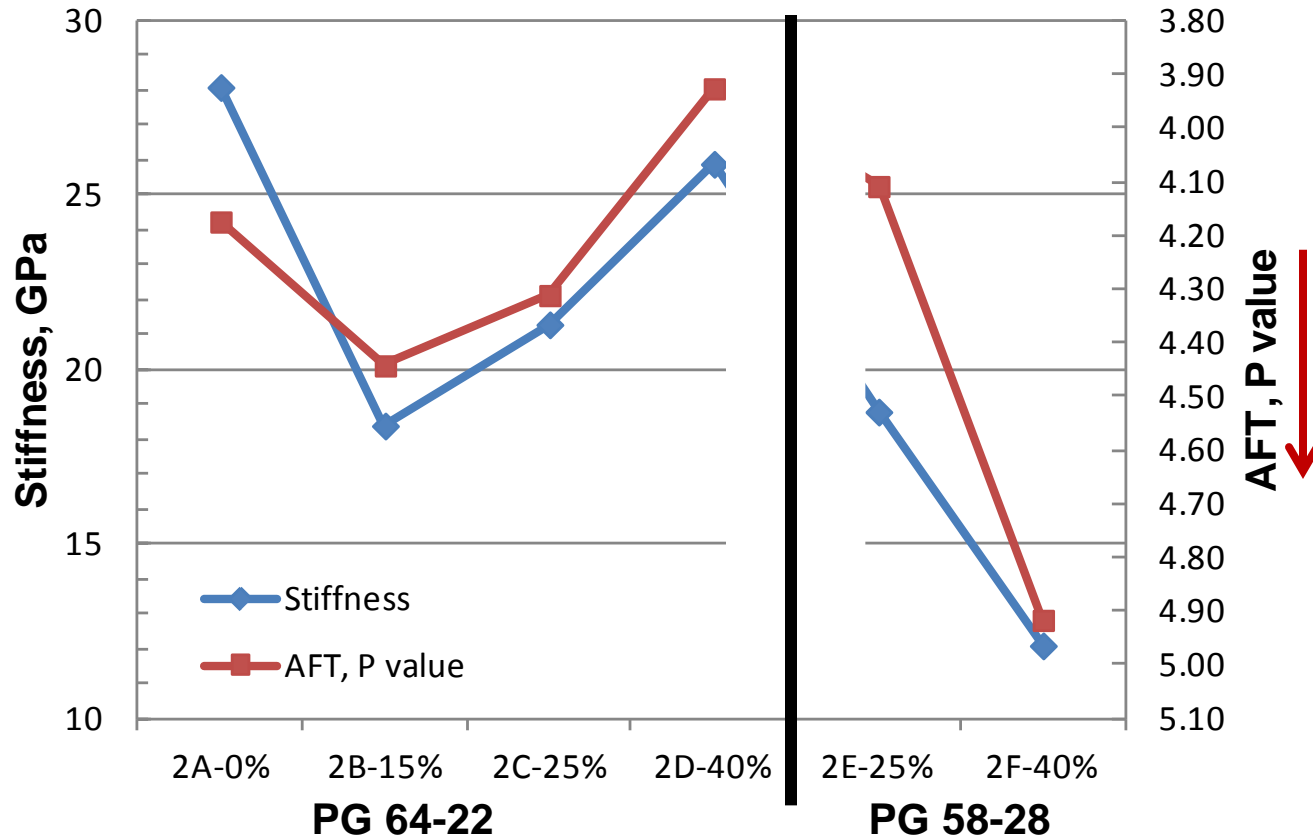
	AFT P-value
AAC-1	4.58
+50% Man RAP	3.86
100% Man RAP	3.78

Semi Predictable blend

Lower p-value = bad compatibility

Anti-synergy in G^*

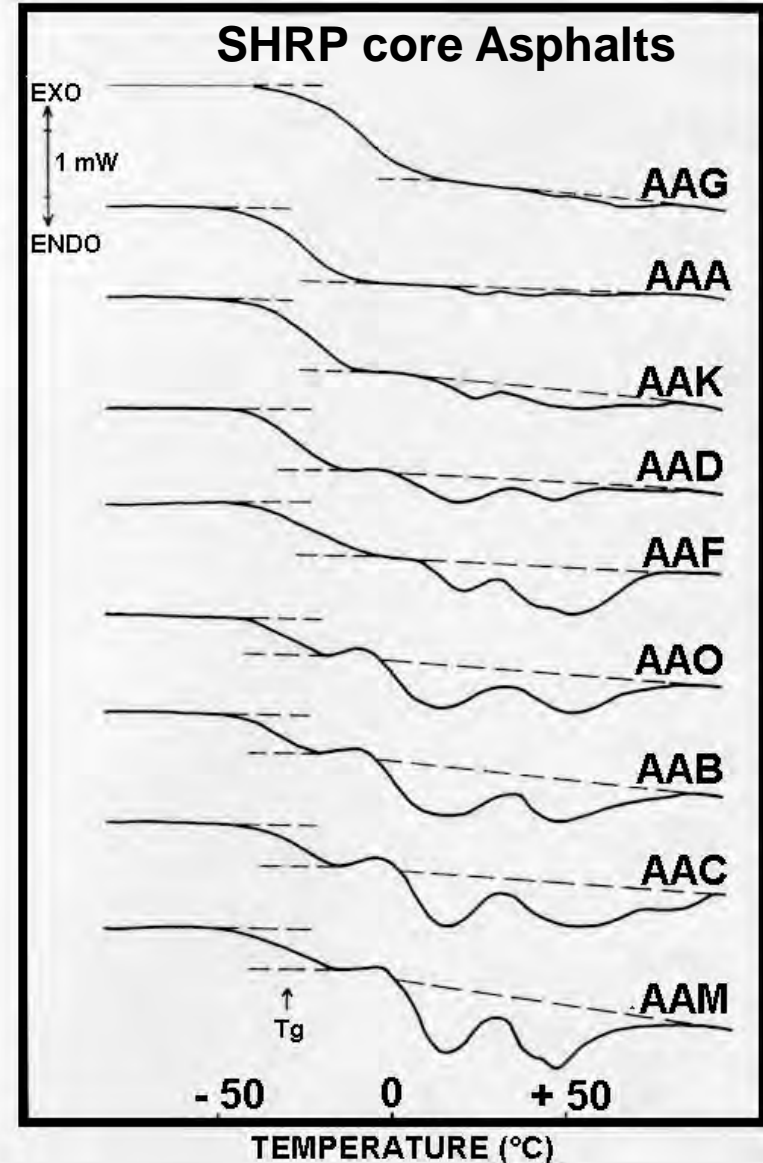
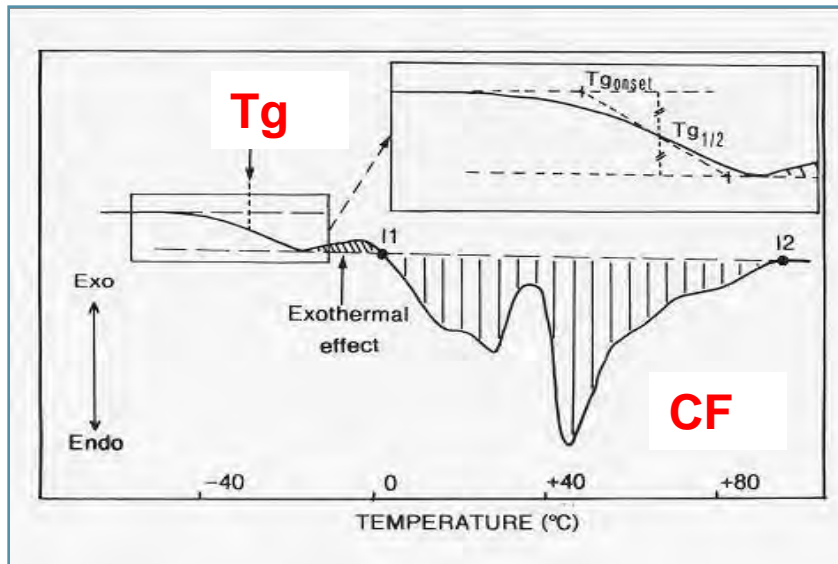
Example 3 : Virgin binder + RAP – Plant blends – IDT mix testing
• PG 64-22 and PG 58-28 with up to 40% RAP / low Temp. E*



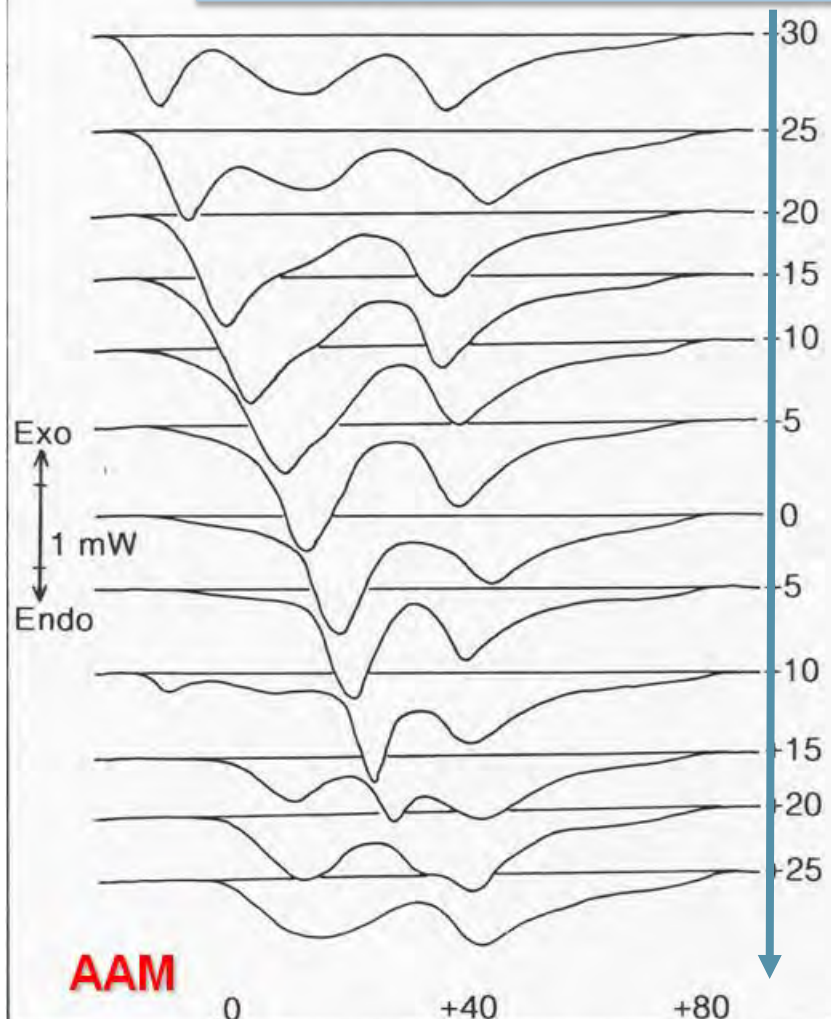
➤ **Mix low temperature stiffness evolution follows AFT p-value**

Data from: *Investigation of Low and High Temperature Properties of Plant-Produced RAP Mixtures Phase II*, McDaniel and Huber

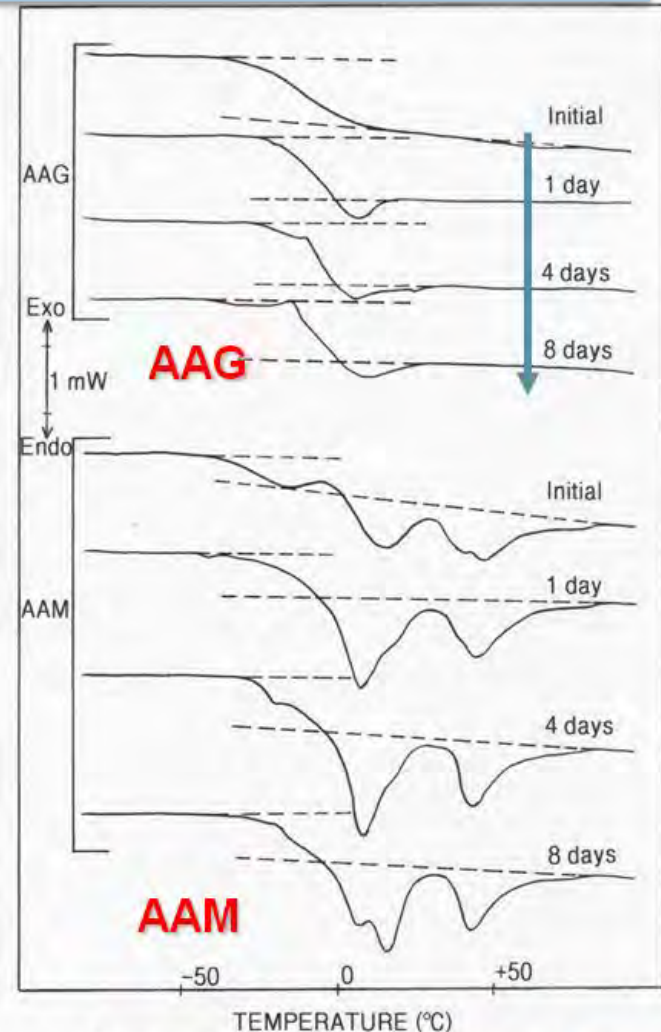
- **Crystallized fraction (CF) present in most Asphalts** not accounted for in the Colloidal model
- **Glass transition temperature not directly used in asphalt models**
- **Differential Scanning Calorimetry**
- **Work by: Claudy and ELF in the 90's and Ensley (80's), Turner at WRI, Masson...**



Asphalt crystallized structure is thermal history dependant

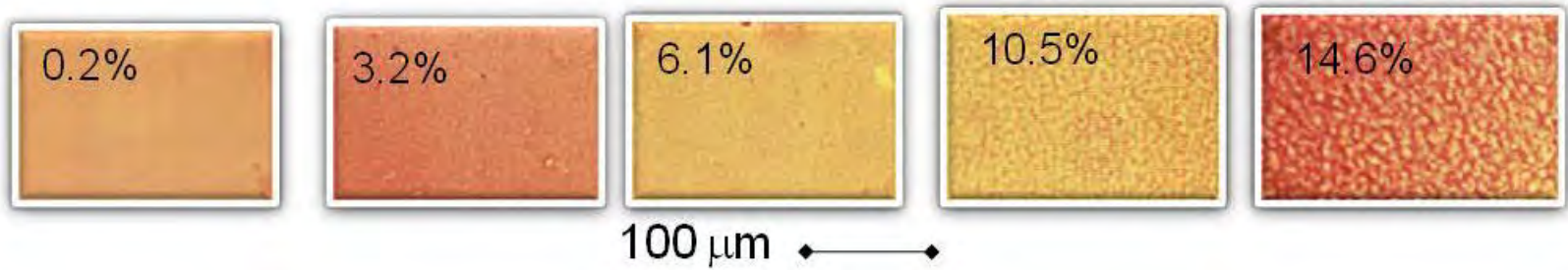


Conditioning **temperature, deg C**

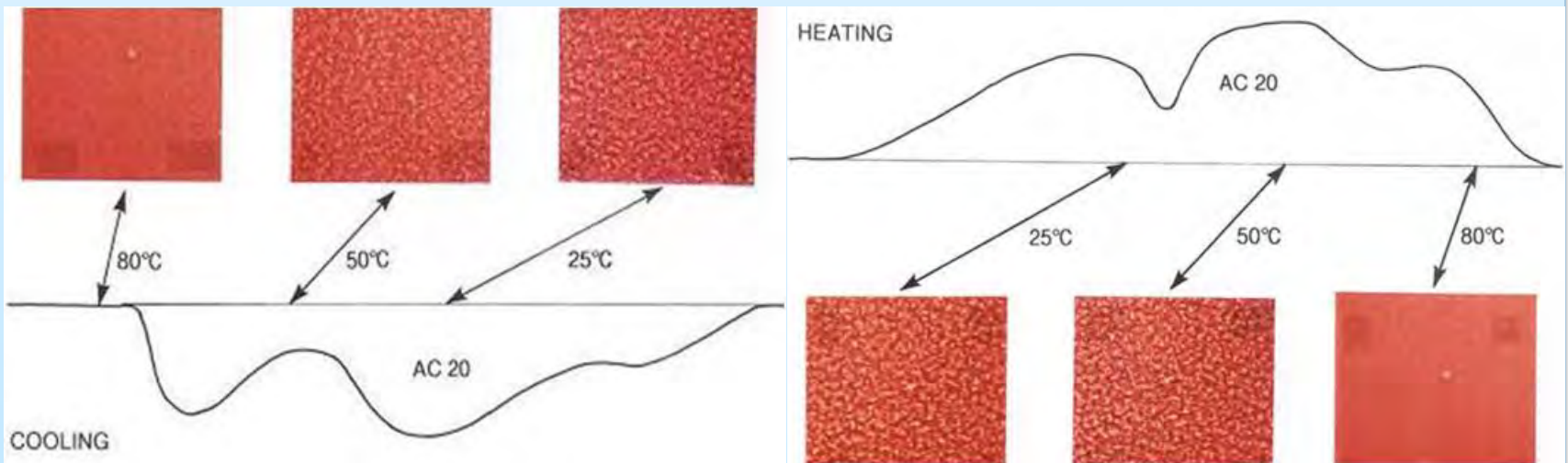


Conditioning **time, days**

- Crystallized Fraction - **Phase contrast microscopy** observation at 25°C for different asphalts

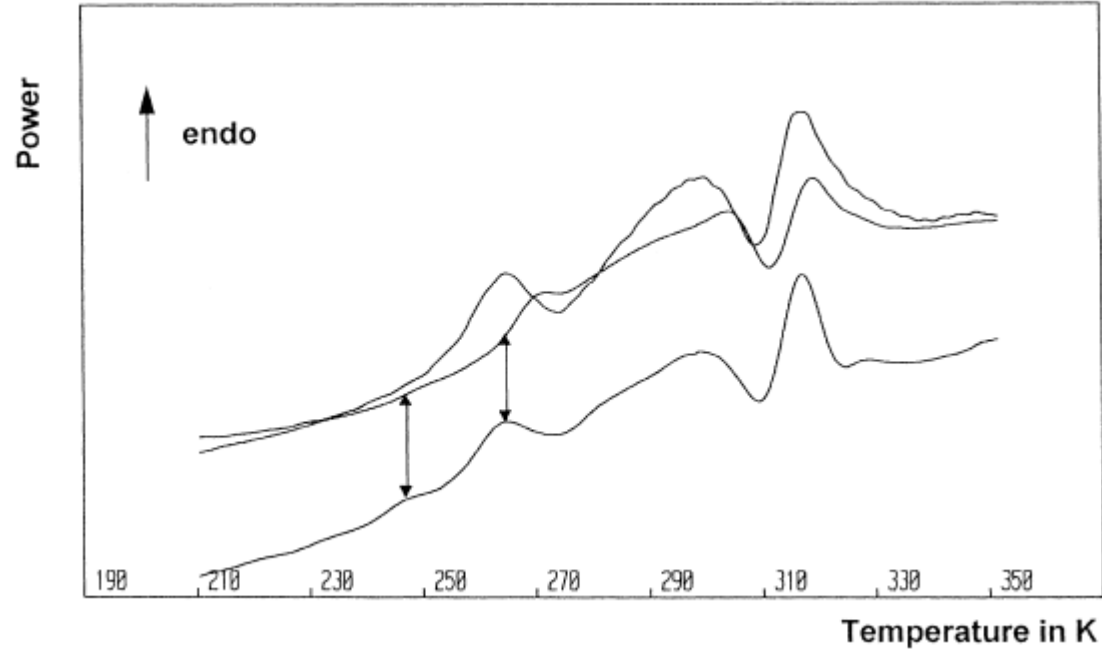


- Crystallized Fraction varies as a function of temperature upon cooling or heating - **Phase contrast microscopy and DSC**



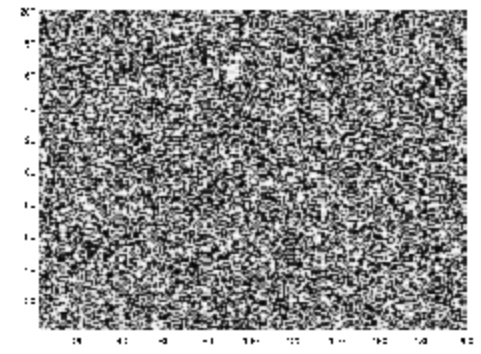
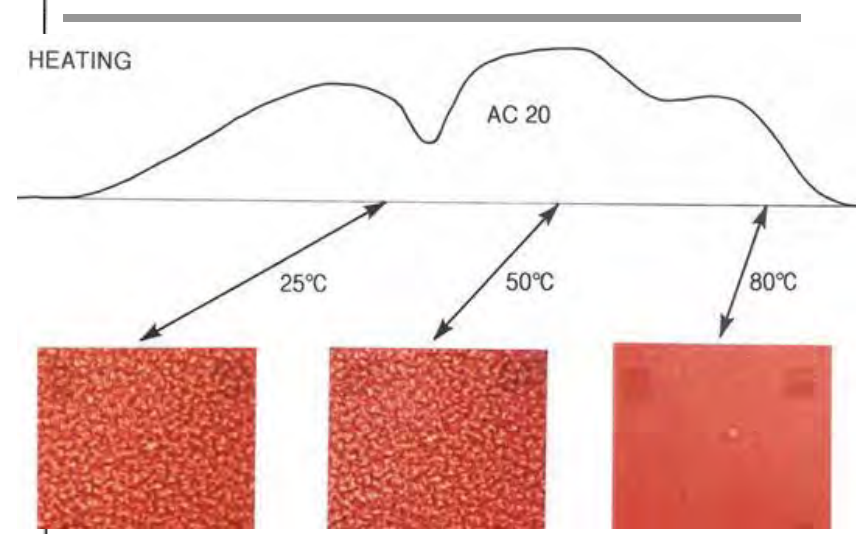
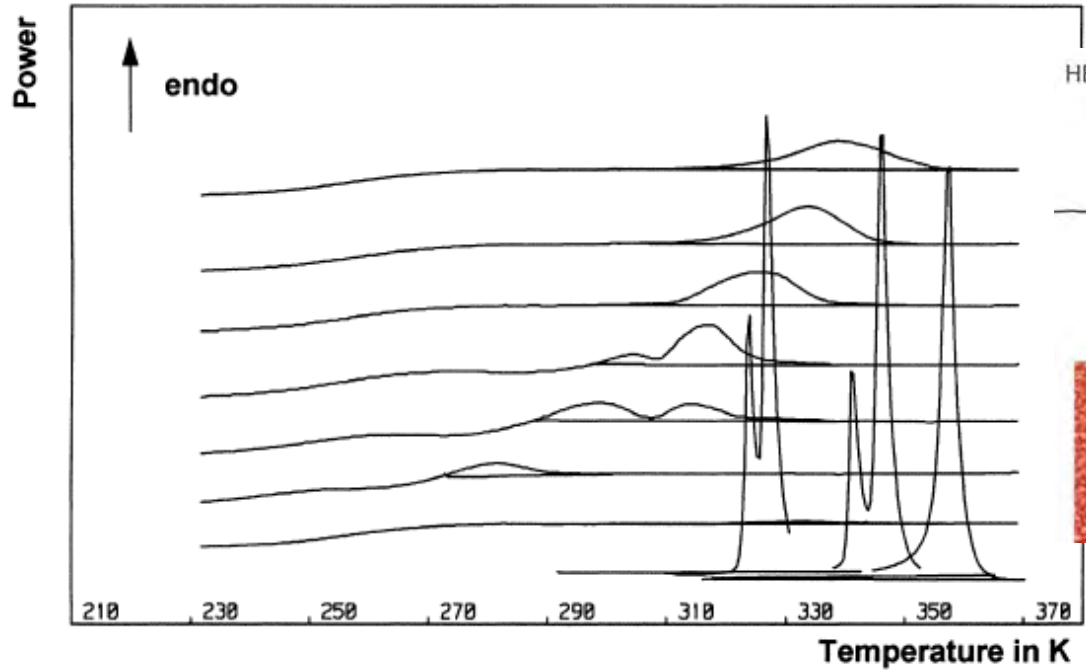
Modulated DSC shows 2 Tg's

- Asphalt conditioning
-30C for 16 hrs
- Heat capacity from
phase shift (b), amplitude
(m), Average signal (t)



- **What's happening?**
- At room temperature: asphalt made of two liquids and some crystallized fractions
- At lower temp: CF increase due to lower solubility in the liquids
 - Two glasses are formed depending on temperature
 - Their proportion depends on the thermal history

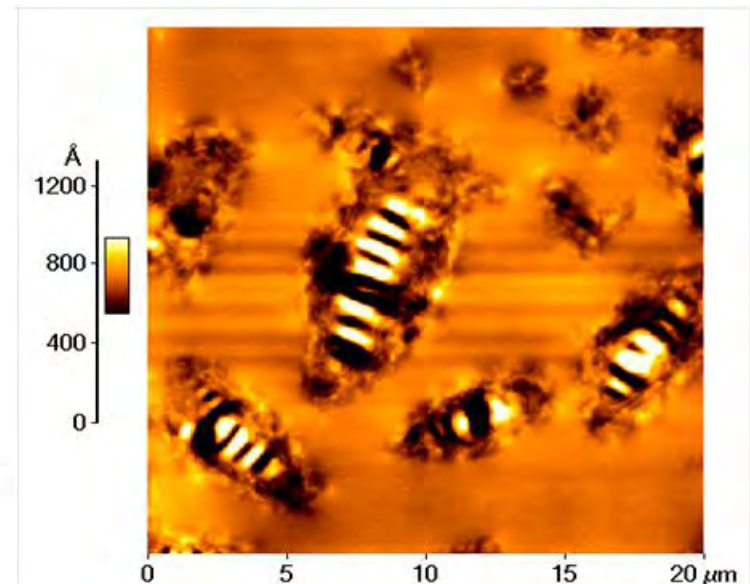
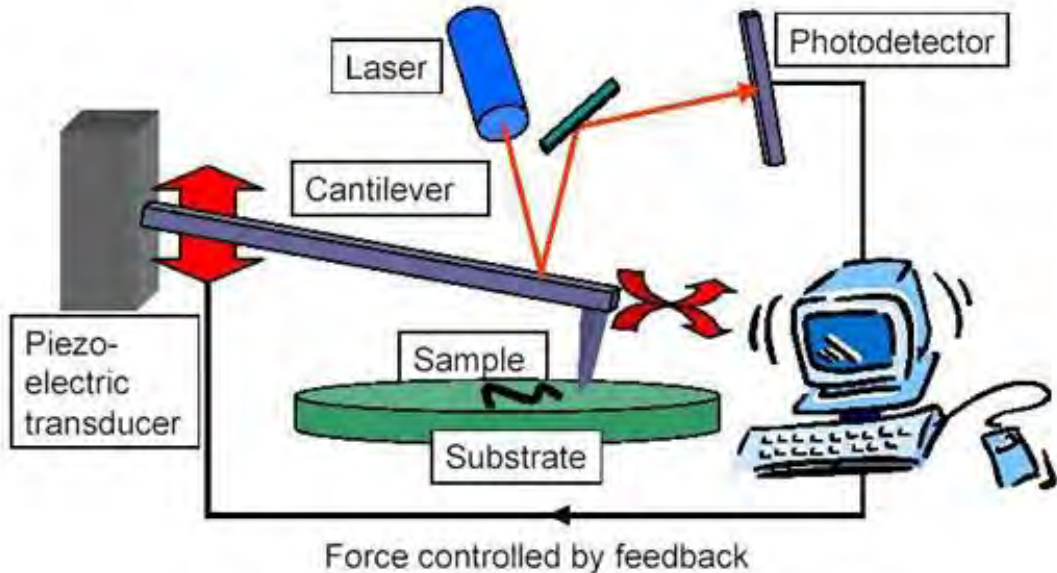
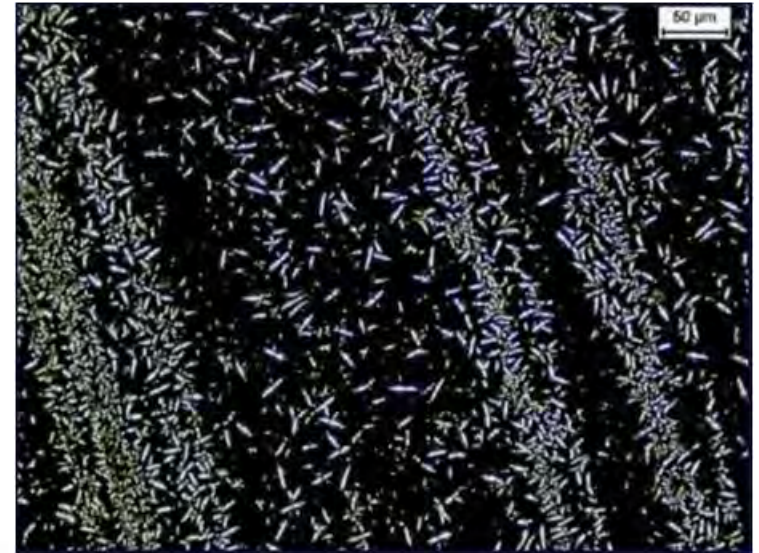
Additions to the colloidal model



- ✓ **Proof of concept by doping n-paraffins in a non waxy asphalt - C20 to C40**
- **Dissolution endotherm at much lower temperature than melting**
- **Crystallized fraction makes asphalt phase separate into 2 liquids as in a spinnodal decomposition –Temp. dependant**

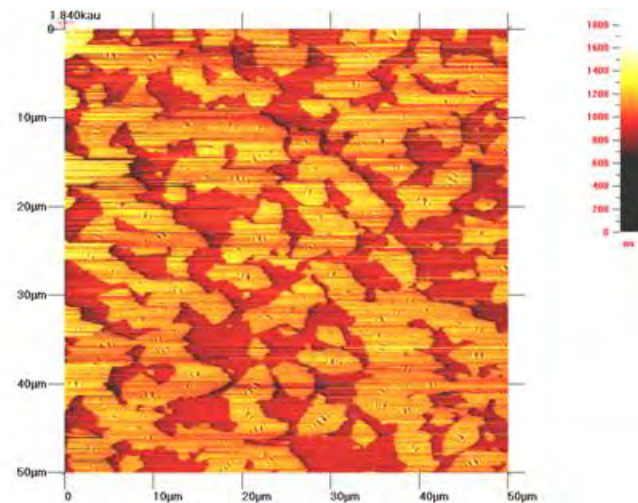
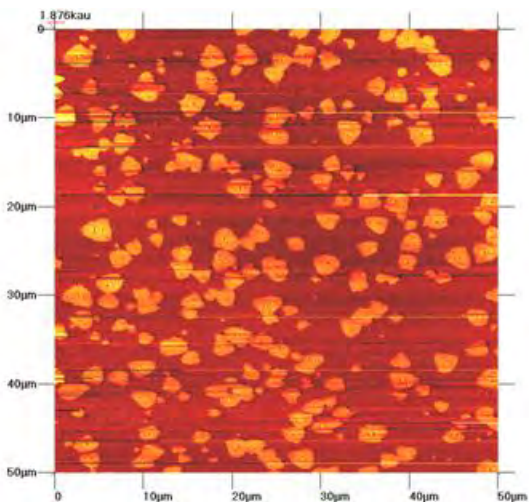
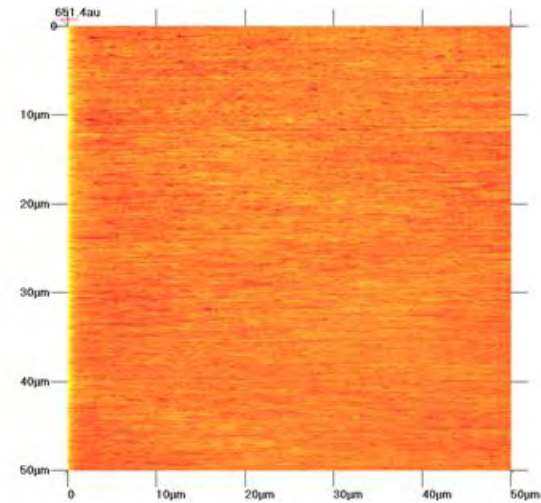
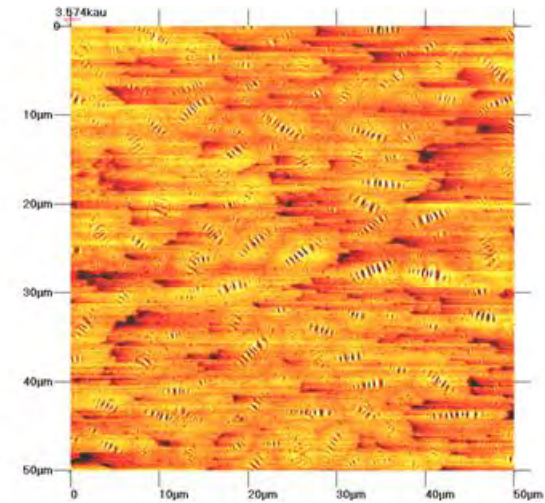
Claudy, *Thermochemica Acta* (1998)
Wikipedia

- **Cold surface crystallization of waxes observation**
 - Dark Field Optical Microscopy
500 μm level: Crystals
 - Atomic Force Microscopy
20 μm level: Bee structure

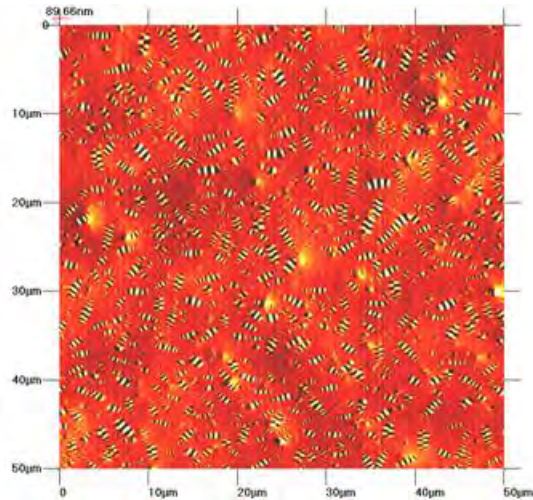


- **Interactions between crystallizing paraffin waxes and the non-wax asphalt components are responsible for much of the structuring**
 - Including the bee-structures observed on the surface of asphalt thin-film samples by AFM
- **AFM a powerful tool to visualize surfaces at very small scale – BUT tricky...**
 - Sample preparation / Film thickness
 - Thermal conditioning prior and during imaging - Cool rates / Time / Temperature
 - Wax concentration in the bulk
 - Molecular weight distribution of wax
 - Properties of the medium from which wax crystallizes from (e.g., asphalt crude source or asphalt fraction)
- *Troy Pauli's dissertation, March 2014*

Bee Structuring as a function of crude source

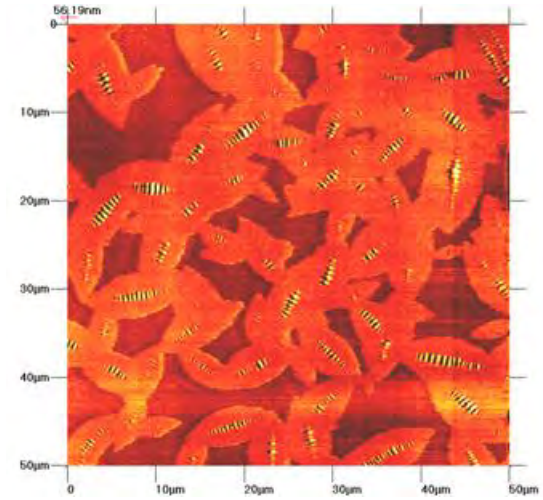


Bee Structuring as a function of chromatographic fraction – interactions with the various fractions

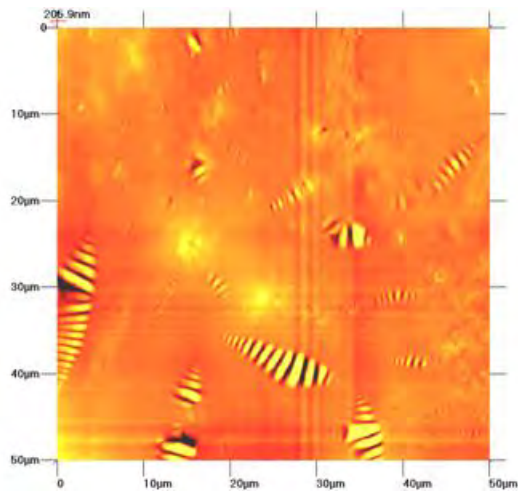


AAB-1-Neat

At 25°C

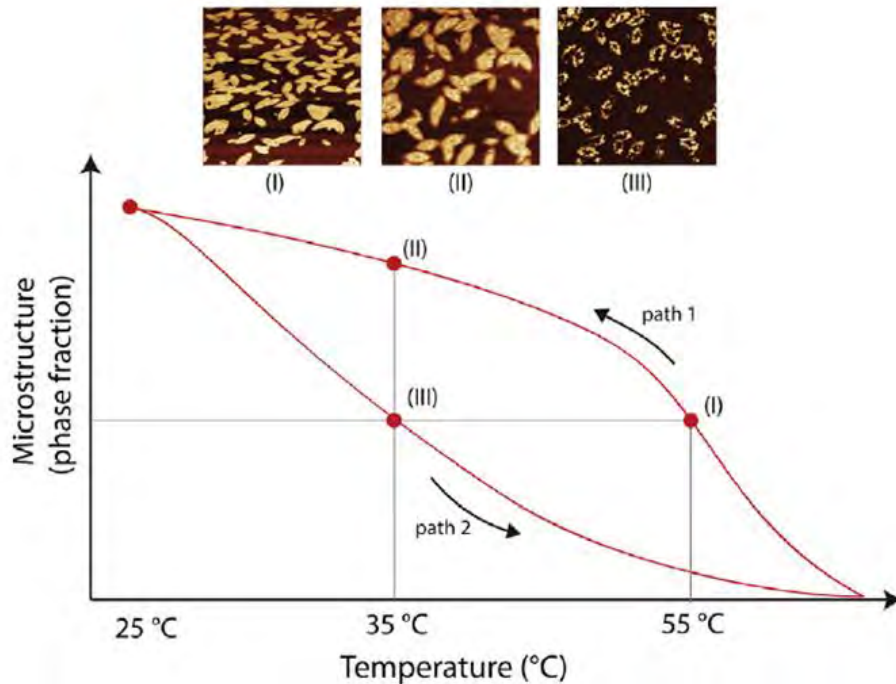


AAB-1-Maltenes



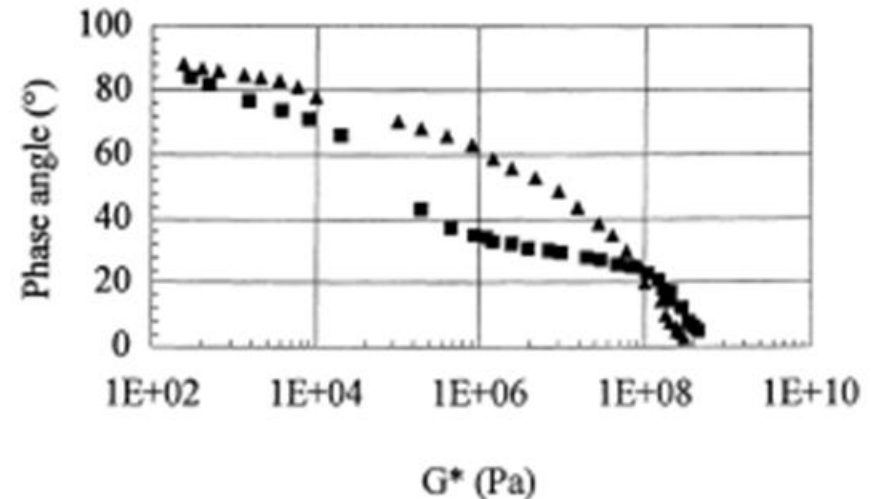
AAB-1-Neutrals

Thermal hysteresis of the microstructure morphology of bitumen



TU-Delft Works (2010's)

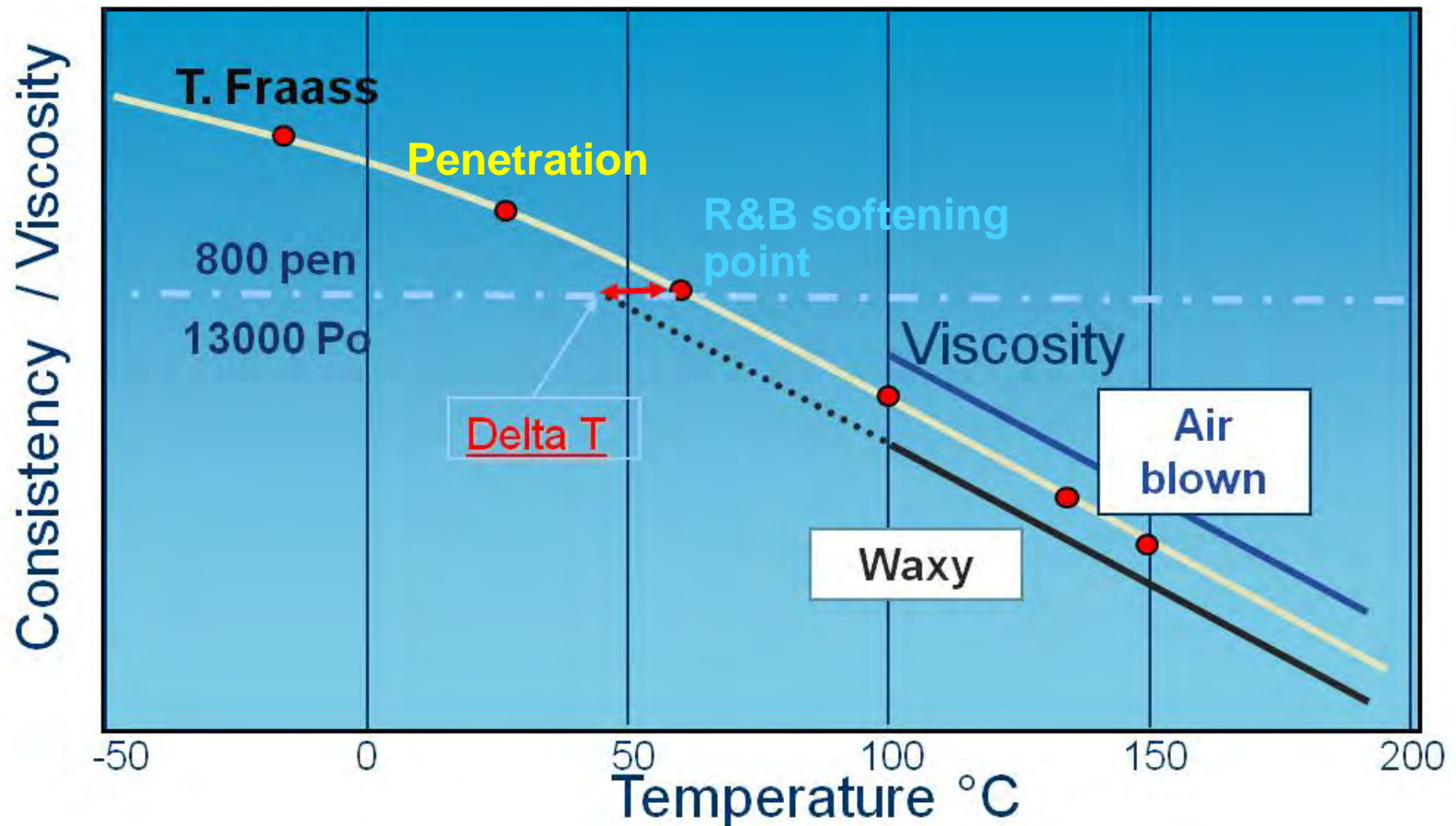
Thermal hysteresis of the rheology of waxy asphalts (comparison 3% vs. 10% CF asphalts)



TOTAL (Elf) Works (1990's)

Relationships between Asphalt Structure & Mechanical properties

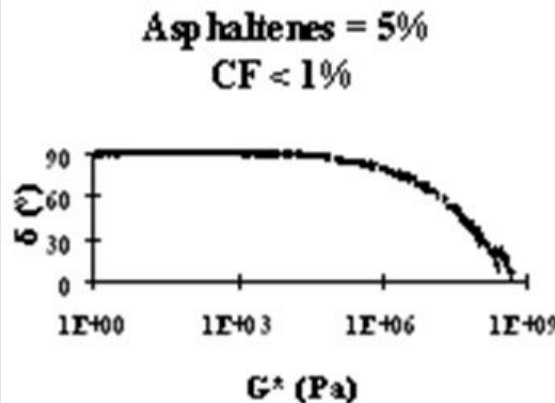
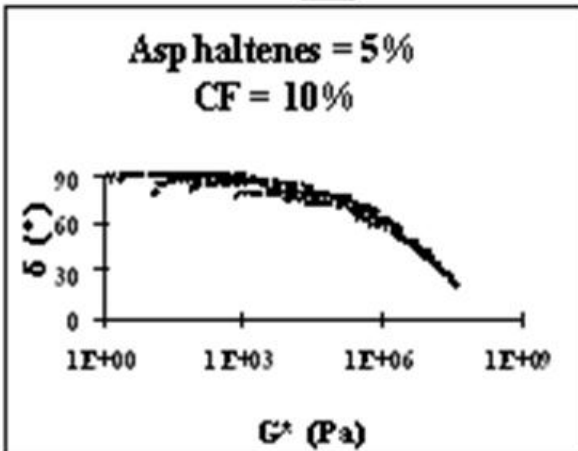
W. Heukelom, 1973



Relationships between Asphalt Structure & Mechanical properties

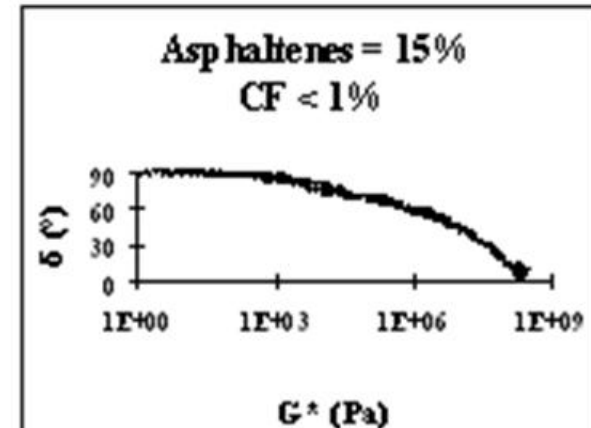
- Time Temp Superposition Principle applicability ?
 - YES: single curve in case of “Sol” structures
 - NO: “Gel” structure / high wax or high asphaltene contents
- Dynamic Shear Rheology using Black space - no data shift
 - Phase angle as a function of the stiffness modulus
- Works: Ramond, Such (LCPC) in the 80’s, Lesueur, Champion-Lapalu (Elf) in the 90’s

High Crystallized fraction



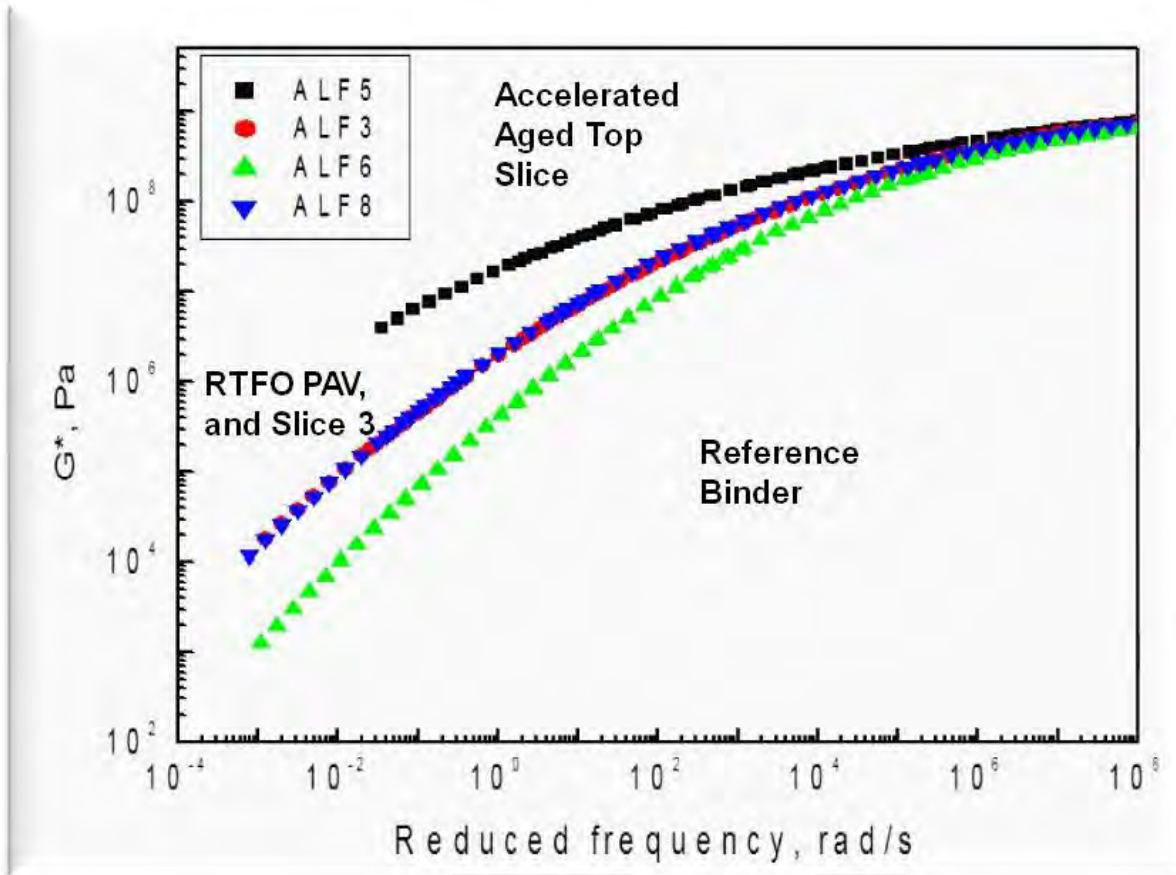
Rheologically simple
-> Low Asphaltene & wax

High Asphaltene



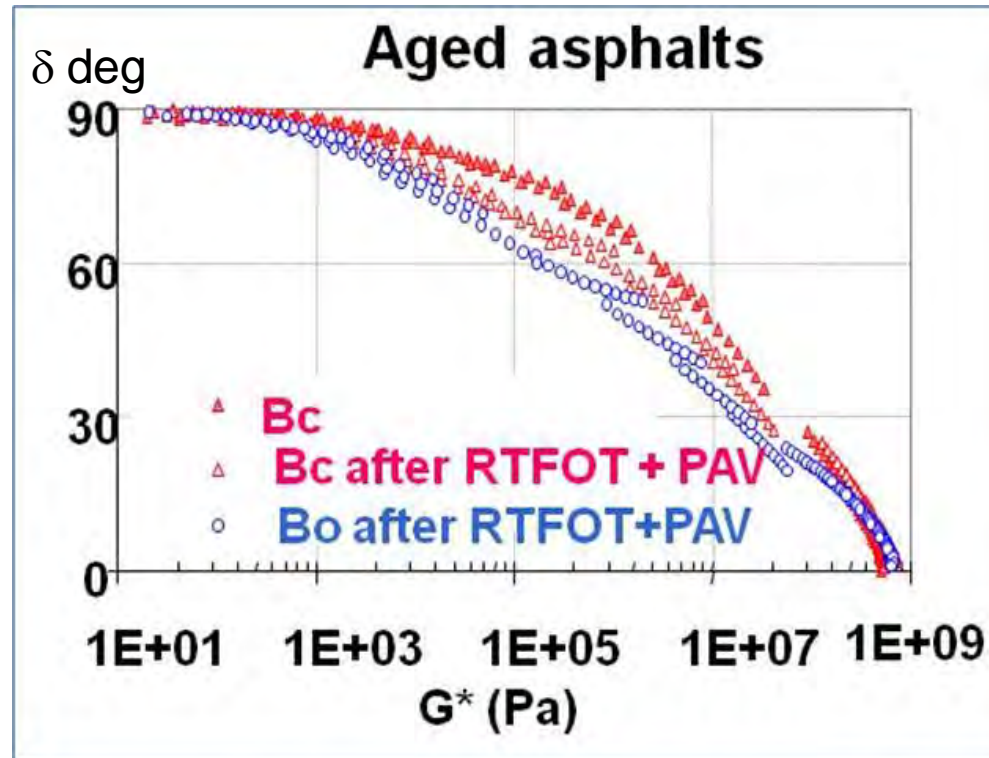
Relationships between Asphalt Structure & Mechanical properties

Typical effect of ageing on asphalt rheological properties



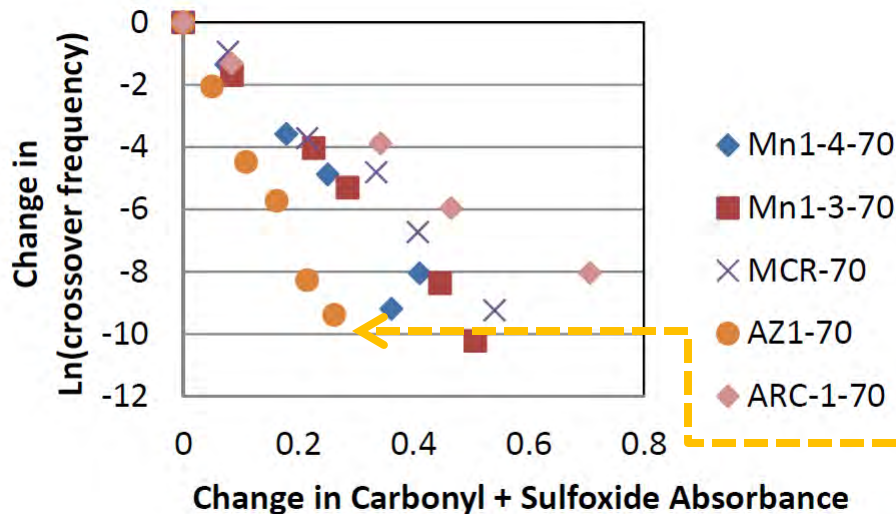
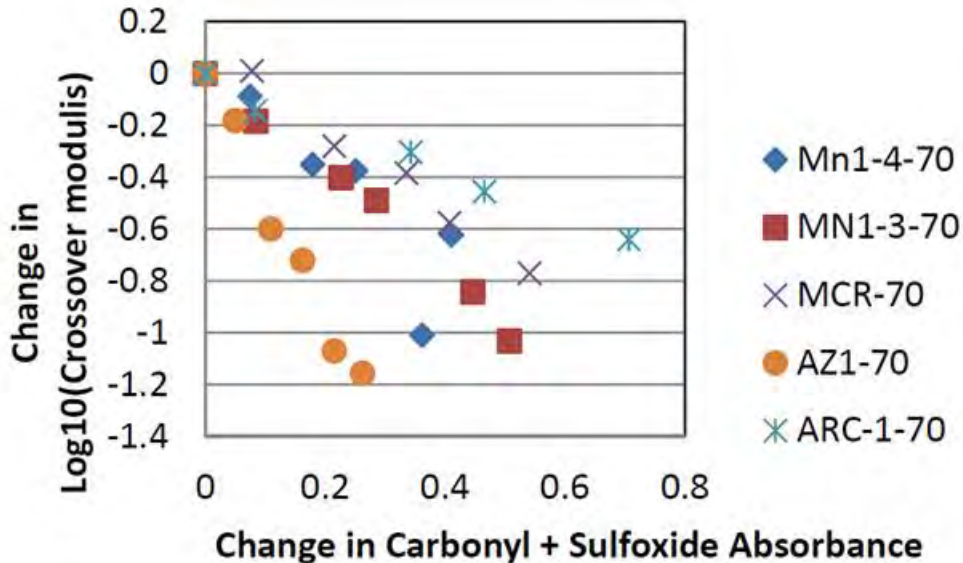
Stiffening:
Increase in
stiffness modulus

Relationships between Asphalt Structure & Mechanical properties



- More in depth effect of oxidative aging: stiffening, more elastic behavior, “flattening” and shift from TTSP
 - Black space visualization
 - Asphaltene increase due to aromatization and polarity
- Works by: Mouillet / Lamontagne (TOTAL/LCPC) - early 2000

Relationships between Asphalt Structure & Mechanical properties



- Binder stiffening upon oxidation tracked by the crossover modulus
 - Parameter where a material goes from elastic to viscous ($\delta=45^\circ$)
- Stiffening rate with oxidation function of binder original state
 - **Gel asphalts stiffen "faster" than sol**
- Farrar and Glaser (WRI-FPIII)

AZ1-70 : Airblown bitumen with a gel structure

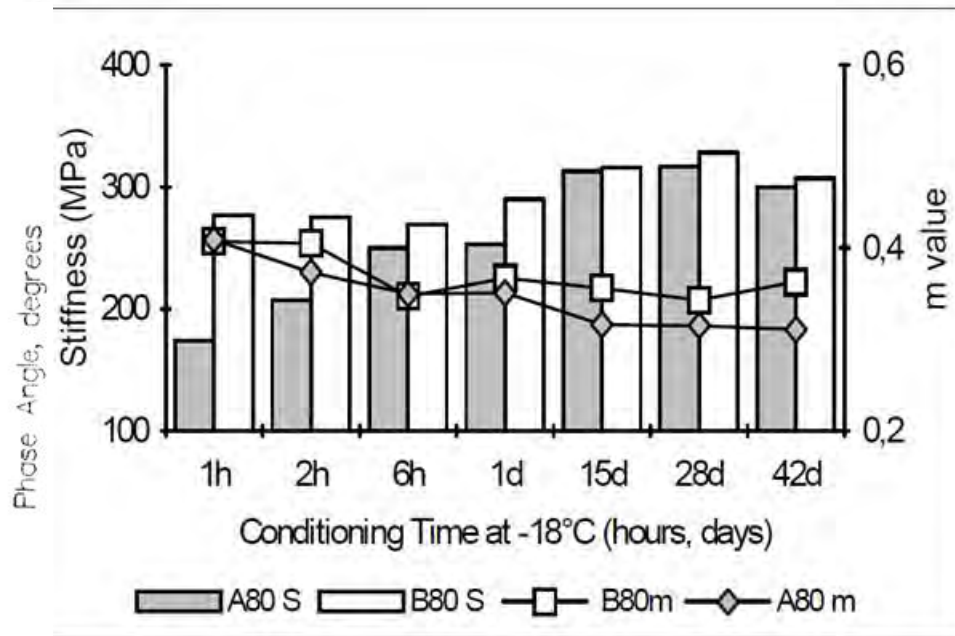
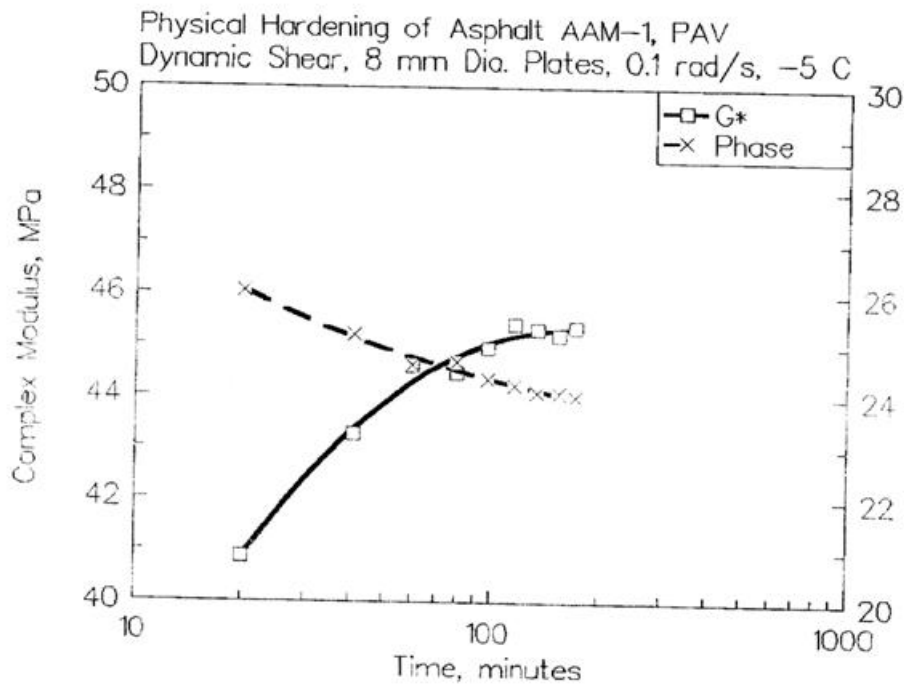
Relationships between Asphalt Structure & Mechanical properties

Physical Hardening by D.

Anderson, H. Bahia (PennState U)

DSR and BBR – SHRP (early 90's)

Physical Hardening in the BBR confirmed by Elf (JP in the 1990's)

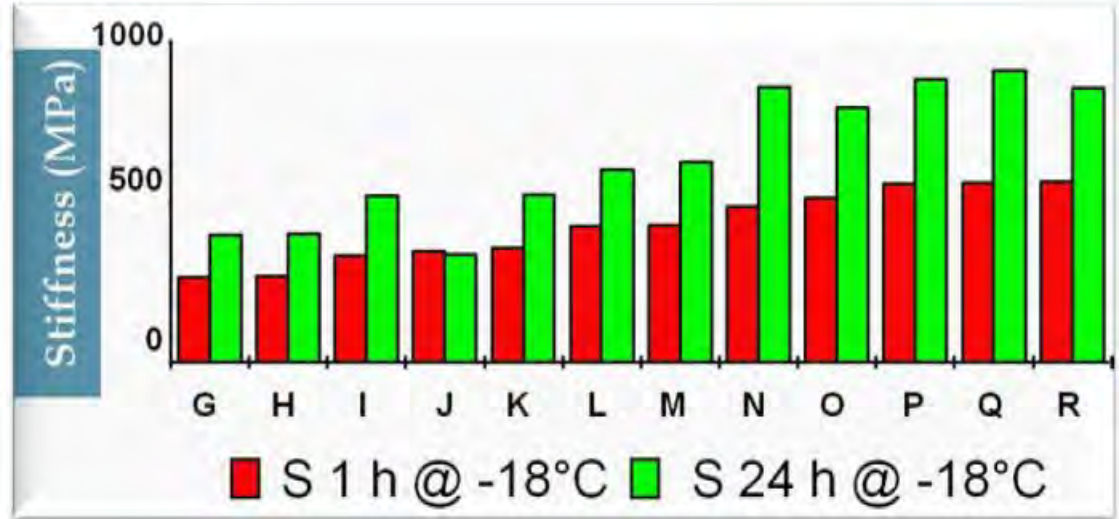
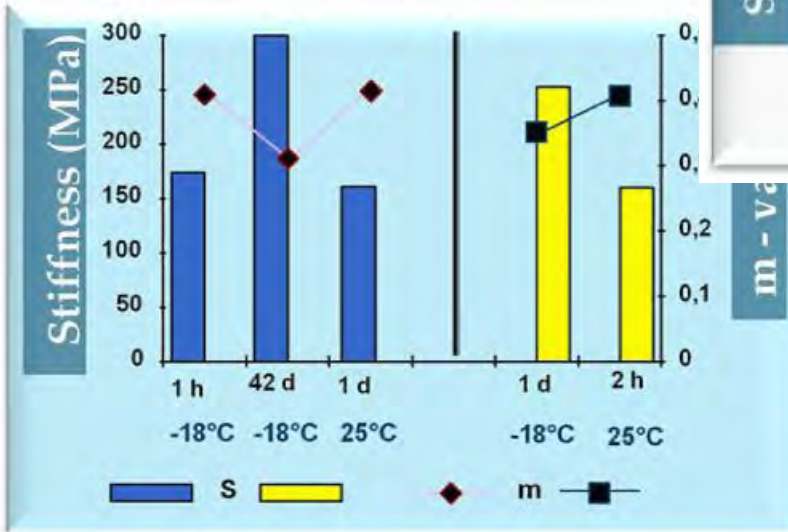


❖ Physical Hardening occurs both in the BBR and the DSR... Intensity and duration may differ

Relationships between Asphalt Structure & Mechanical properties

Physical hardening

- BBR ranking impact



Effect of physical hardening on Bitumen ranking (BBR)

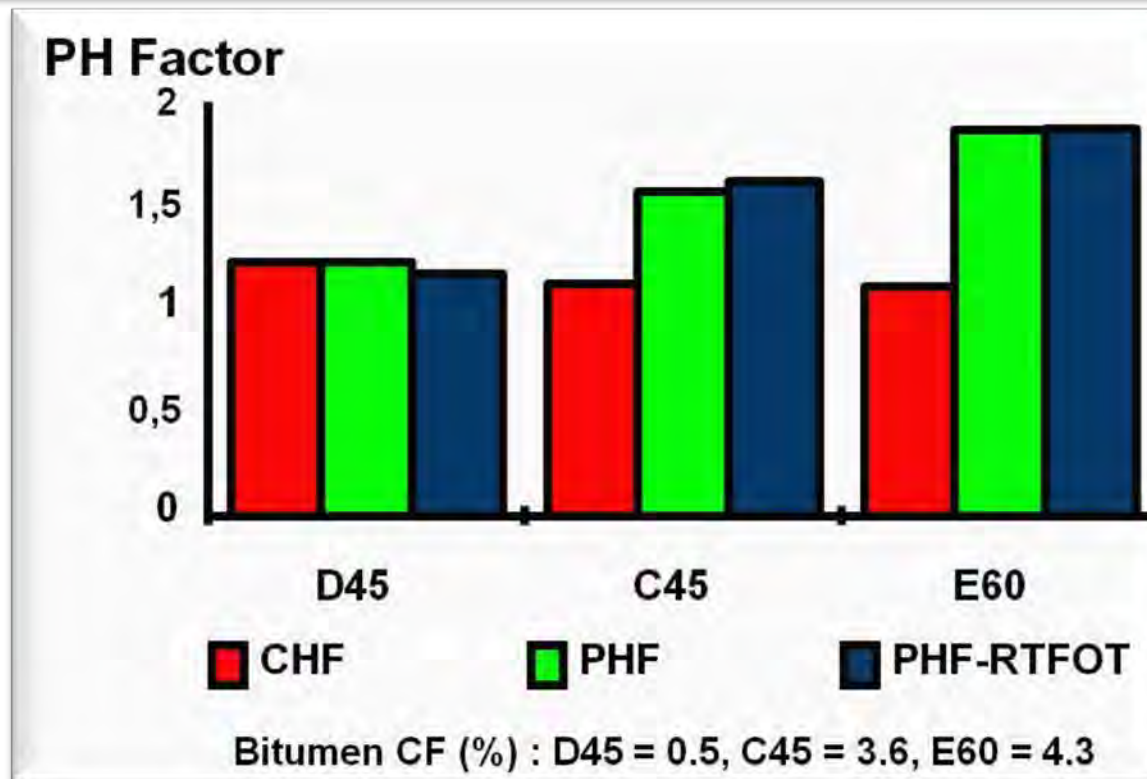
Physical Hardening

- Reversibility at room temperature

Ref: Planche et al, RILEM 1997

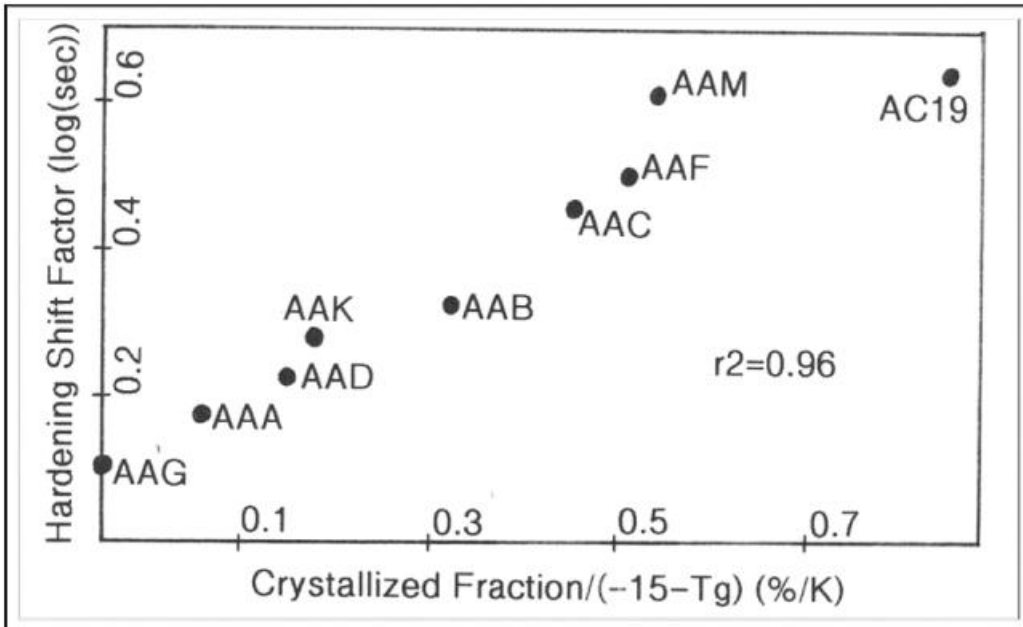
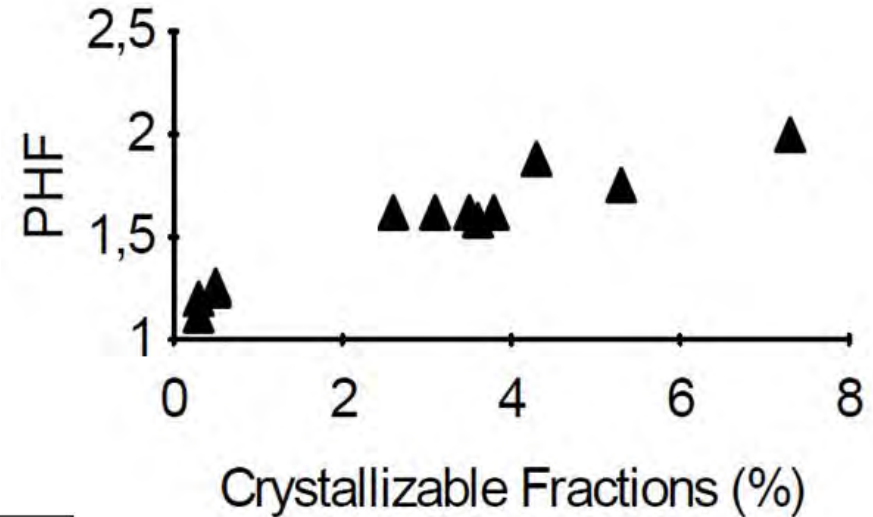
Comparison between Physical Hardening and RTFOT

- Effect at the same level or higher than RTFOT
- Not affected by RTFOT



Relationships between Asphalt Structure & Mechanical properties

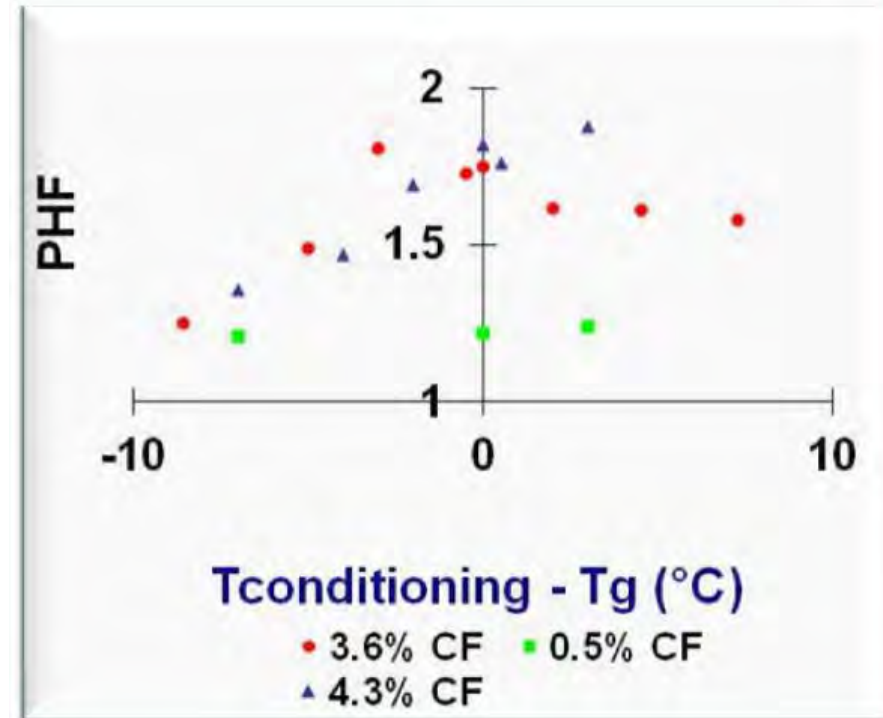
- Physical hardening dependency
 - Crystallized fraction & Tg
 - Conditioning temperature & time
- Assessed by DSC and BBR
- Works by Anderson, Bahia et al (US), Claudy, Planche, (FR) 90's



$$PHF = (S_{24h} / S_{1h})^{(m_{1h} / m_{24h})}$$

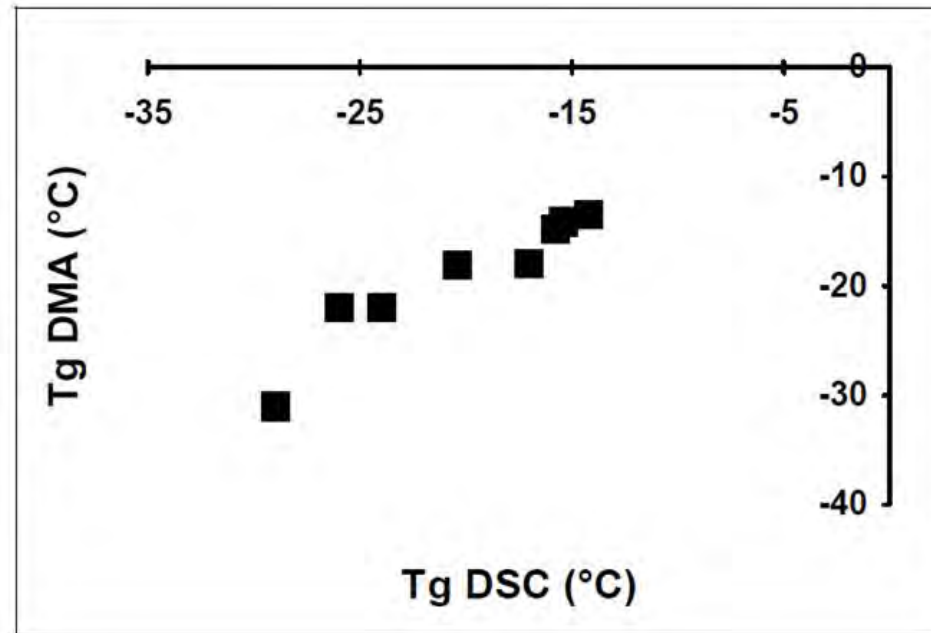
Relationships between Asphalt Structure & Mechanical properties

- **Physical hardening dependency**
 - Crystallized fraction & Tg
 - Conditioning temperature & time
- **Physical hardening reaches maximum intensity around Tg, decreases to nil 10C below Tg**
 - Free volume collapse and wax cold crystallization
- **Assessed by DSC and BBR**
- *Works by Anderson, Bahia et al (US), Claudy, Planche, (FR) 90's*



$$PHF = (S_{24h} / S_{1h})^{(m_{1h} / m_{24h})}$$

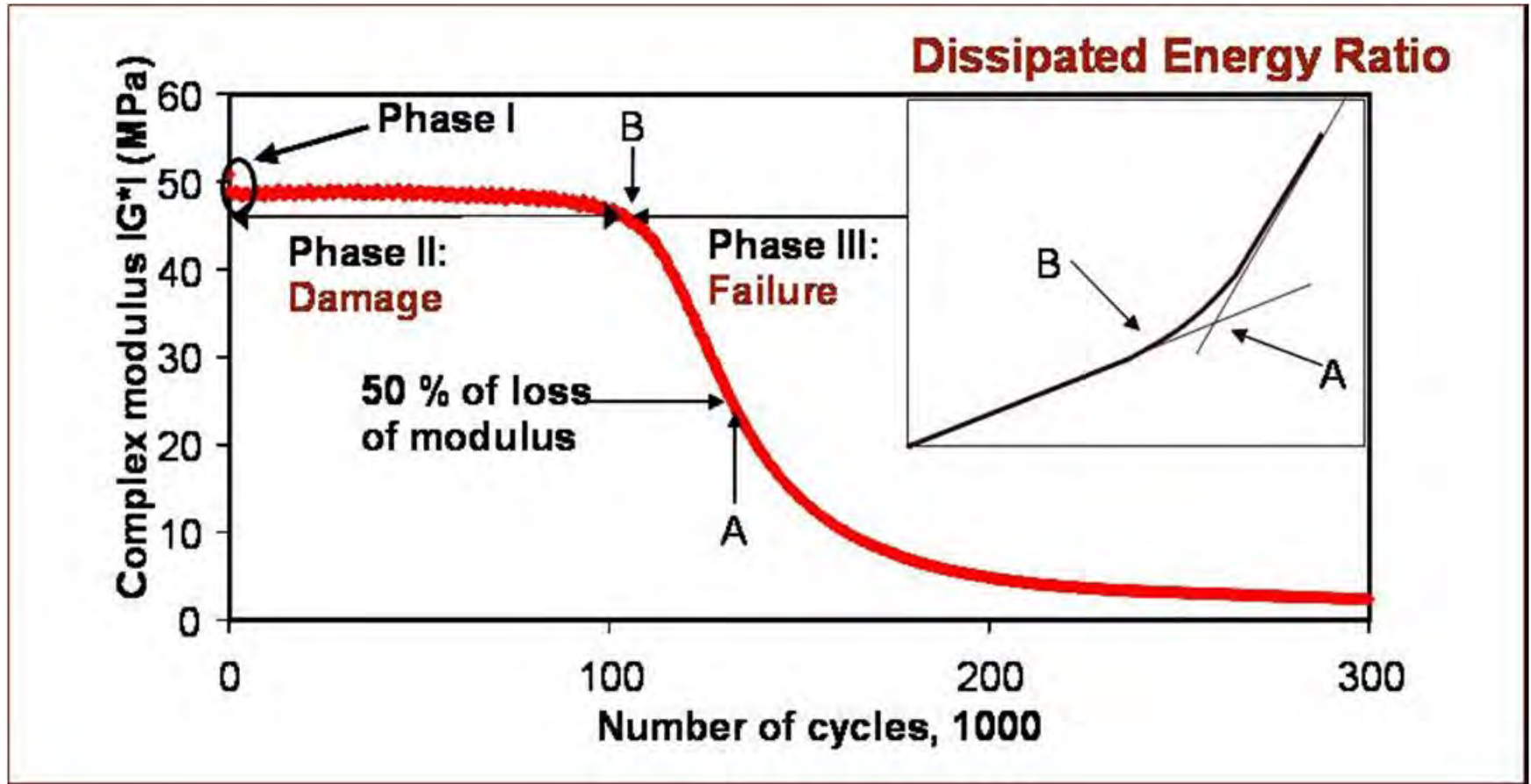
Relationships between Asphalt Structure & Mechanical properties



Relationship Rheological Tg (DSR) vs. Thermal Tg (DSC)

- DSR Tg = loss modulus peaks at low frequency (5 rad/sec)
- Compatibility related blending rules for PMA's and RAP blends
- Related to TSRST critical cracking temperature
- Changes with aging (widened temp. range)

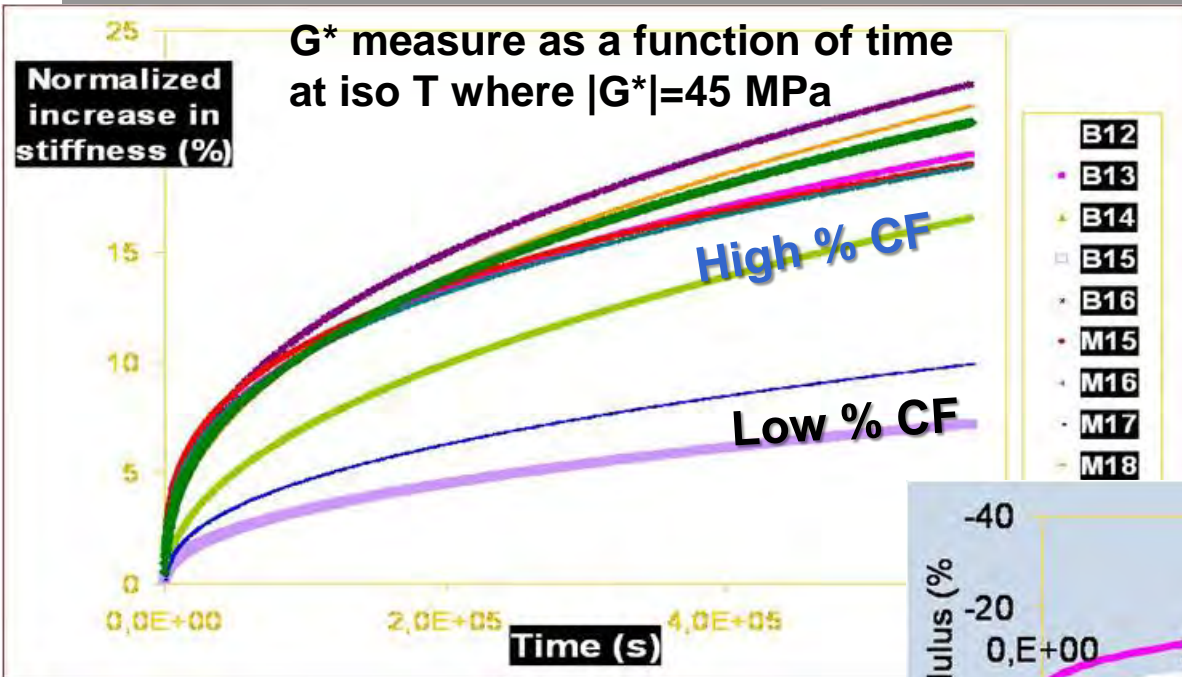
Relationships between Asphalt Structure & Mechanical properties



Fatigue Testing of binders assessed by **DSR Time sweep**

• Work by H. Bahia (UWM), D. Anderson (PennState) and Le Hir, Gauthier (TOTAL) late 90's (US-FR)

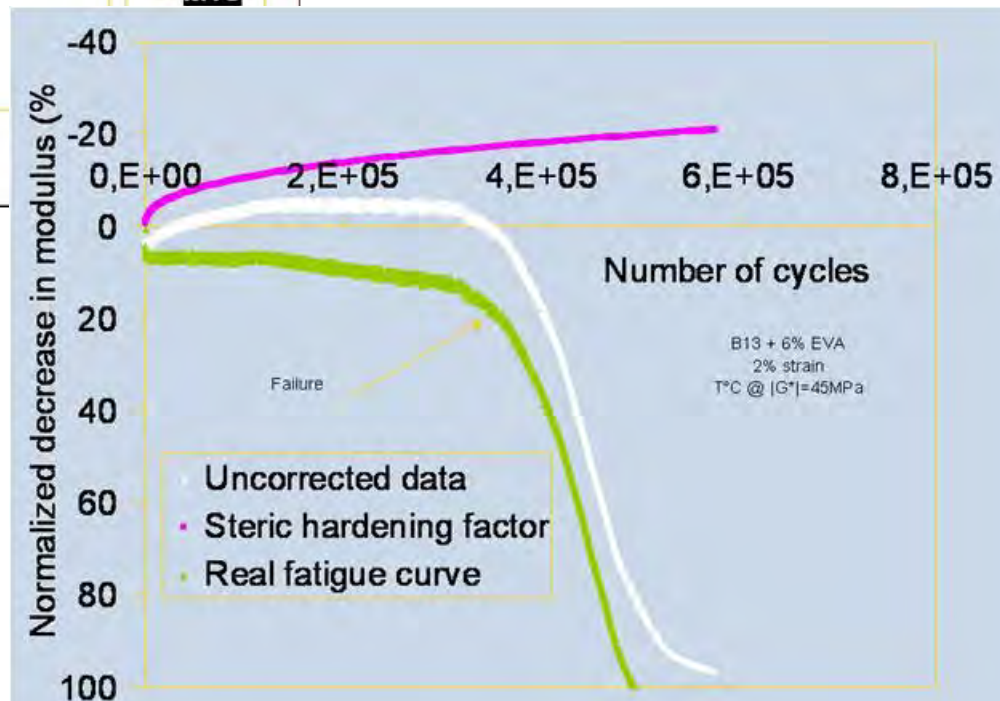
Relationships between Asphalt Structure & Mechanical properties



Time sweep at iso T storage where $|G^*|=45$ MPa

• Influence of Steric Hardening on **DSR time sweep**

- remains under shear
- influences fatigue results
- somehow related to crystallized components



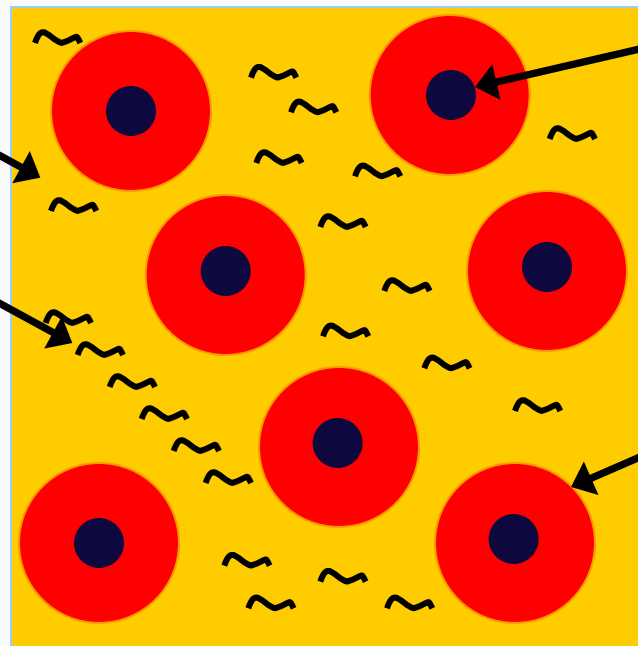
Colloidal suspension of asphaltenes in a maltene matrix

Maltenes
In 2 liquids

Crystallized
fraction

Depending on :

- Crude oil origin
- Temperature
- Aging stage
 - Tank (unaged)
 - Short Term (aggregate mixing)
 - Long term - in service in the pavement
- **Presence of an additive or a polymer**



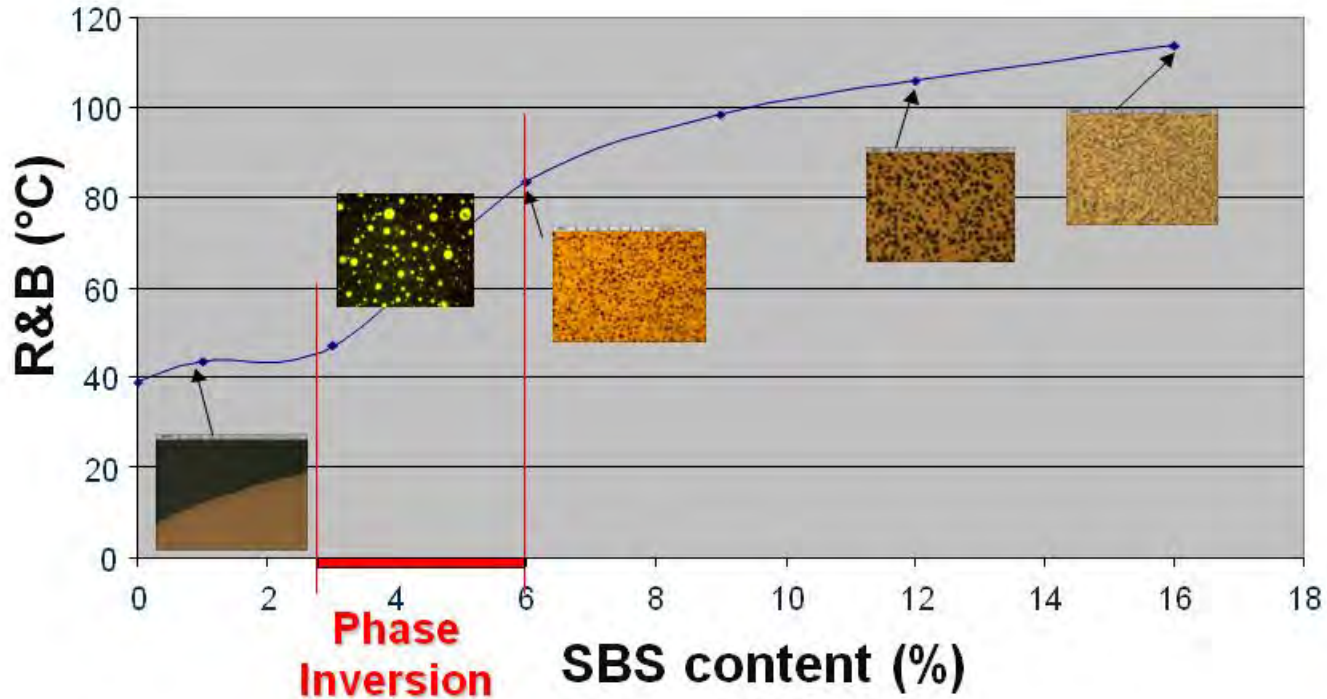
Asphaltenes

Resin layer

- **Background - Context**
- **Chemical-physical and structural properties of asphalt**
 - **Impact on asphalt mechanical properties**
- **Asphalt modification**
 - **Impact on structure and mechanical properties**
- **Summary**
- **Perspectives**



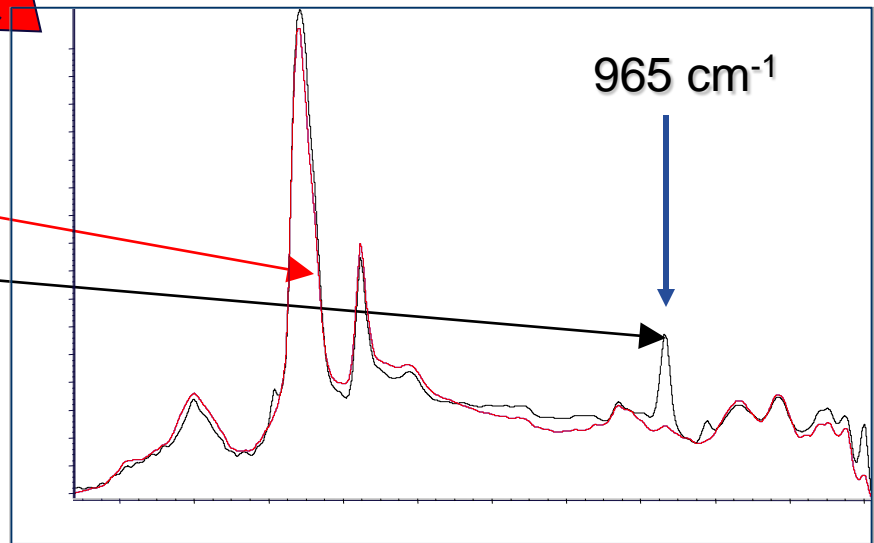
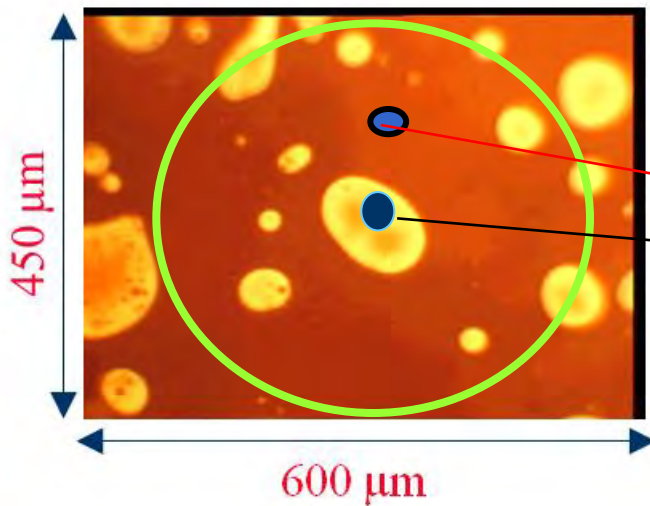
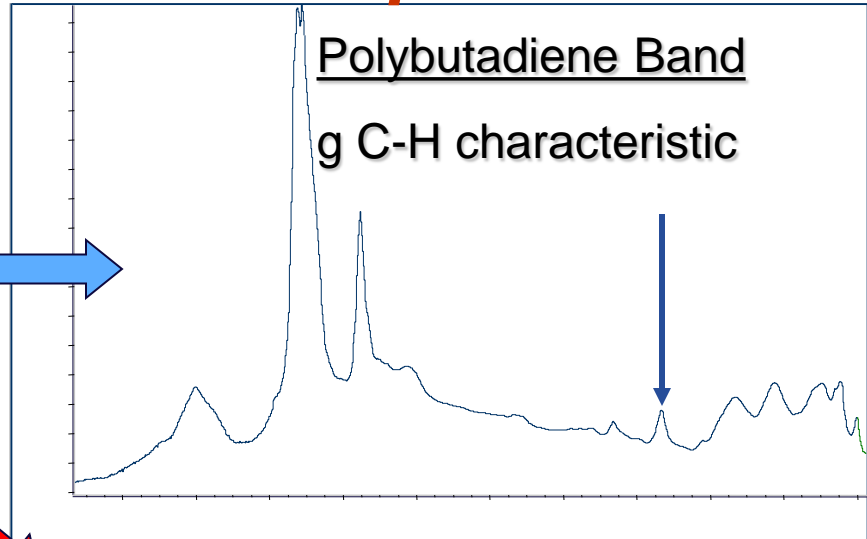
Effect of additives on of Asphalt Structure



- Effect of polymer modification on microstructure & properties - **UV fluorescence microscopy** visualization
 - Polymer swells with light aromatic oil maltenes
 - Polymer phase inversion between 3 and 6% polymer
 - Big jump in consistency (R&B softening point, $G^*/\sin \delta$...)
- *Work s: Brule – LCPC (80's) – Shell, Enichem, Elf, Kraton (90's),...*

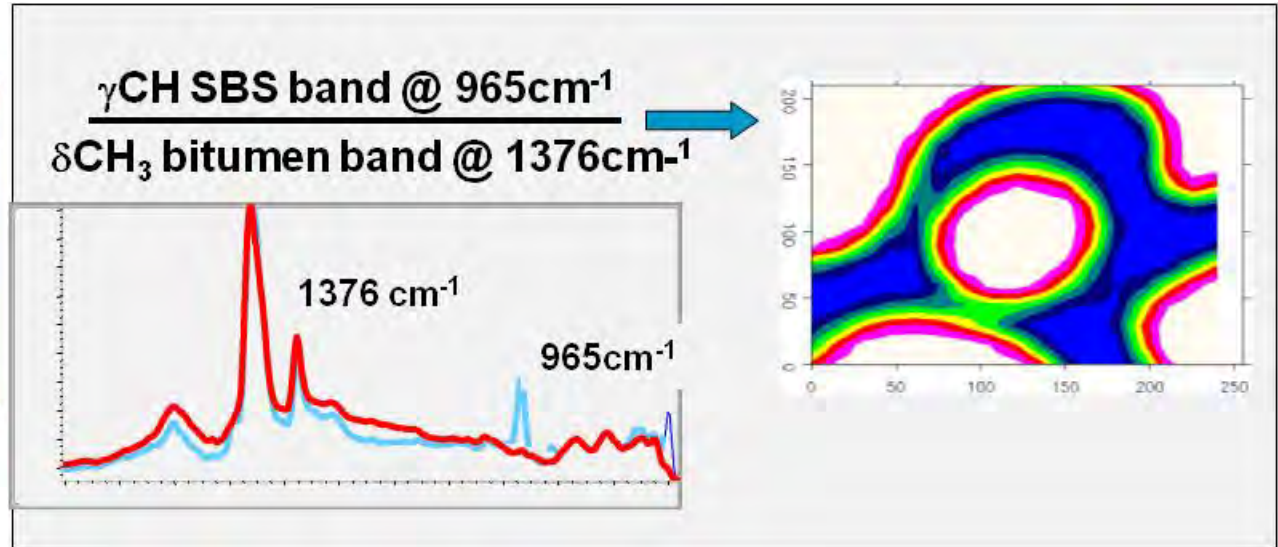
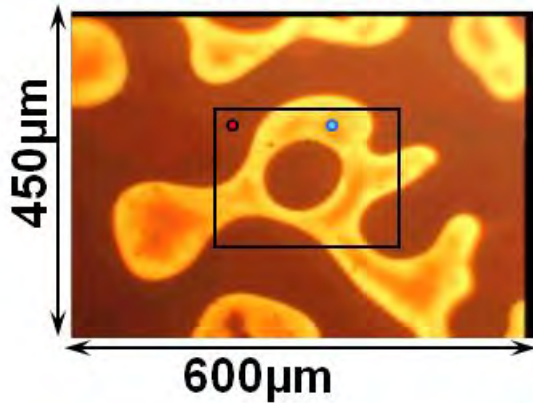
Effect of additives on of Asphalt Structure

- **IR Microscopy** to analyze PMA structure
 - Spectroscopy = Global Analysis
 - IR Microscopy = Local Analysis
- *EU: LCPC-TOTAL-U Marseille in the early 2000, Mouillet et al*

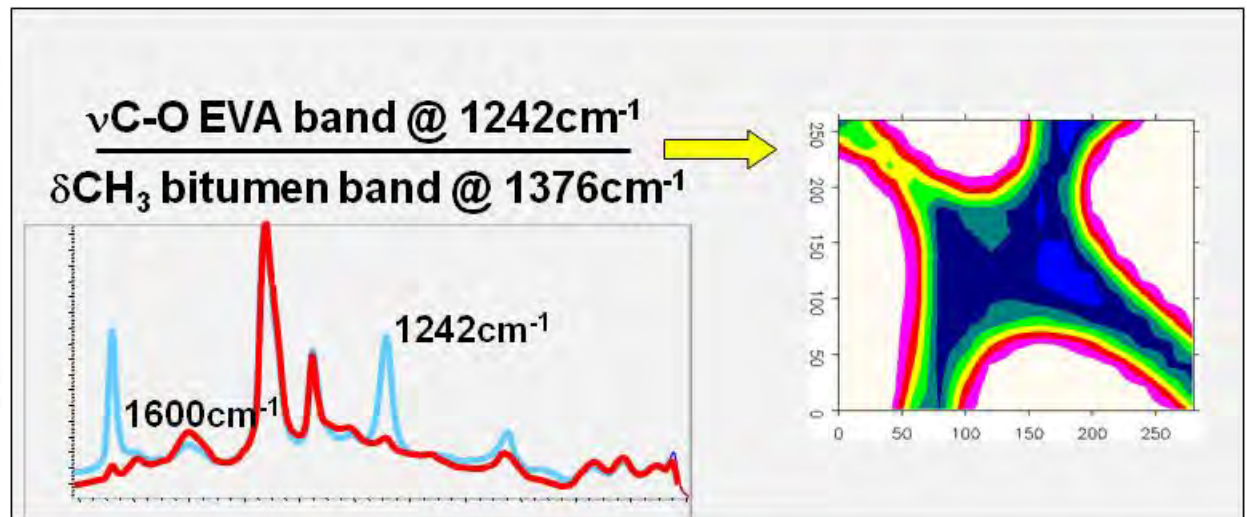
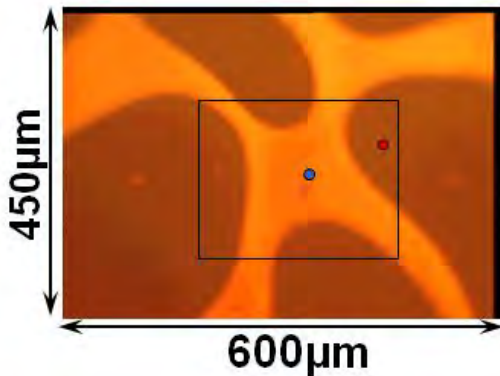


Effect of additives on of Asphalt Structure

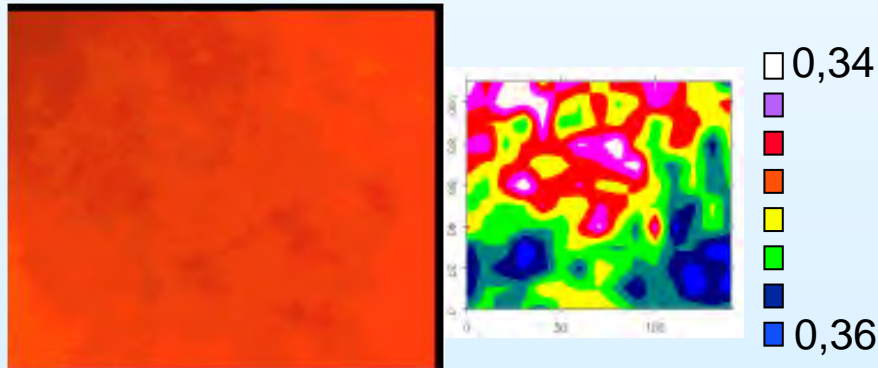
SBS m Bitumen



EVA m Bitumen



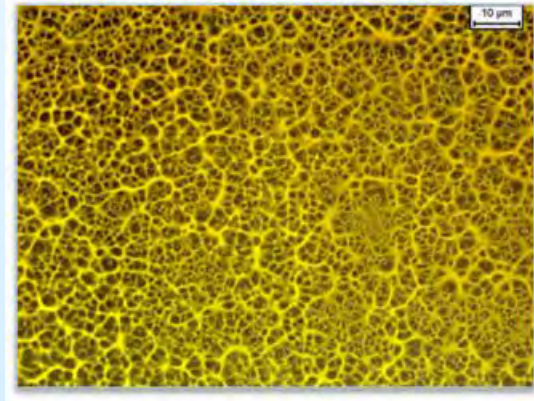
FTIR Microscopy



Fine dispersion of a cross-linked PMA

- ✓ Storage stable
- ✓ Does not evolve significantly during aging
- ✓ Better overall properties

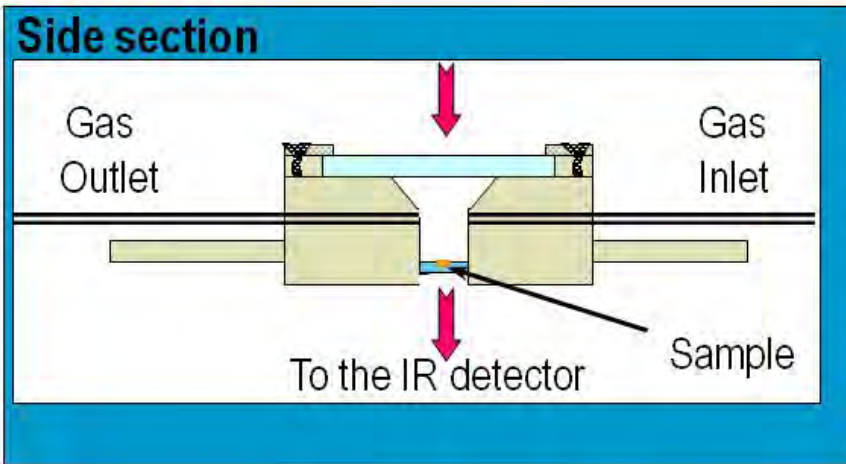
UV epi-fluorescence Microscopy



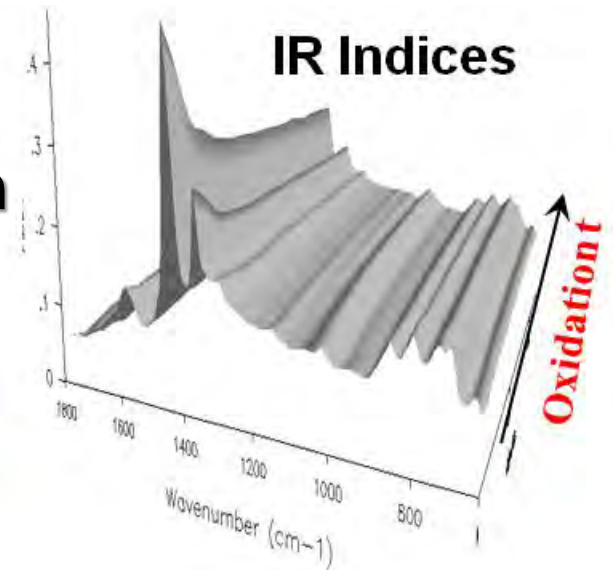
Microstructure of a cross-linked PMA

3 D Network revealed
by N-hexane rinse

Effect of additives and aging on of Asphalt Structure



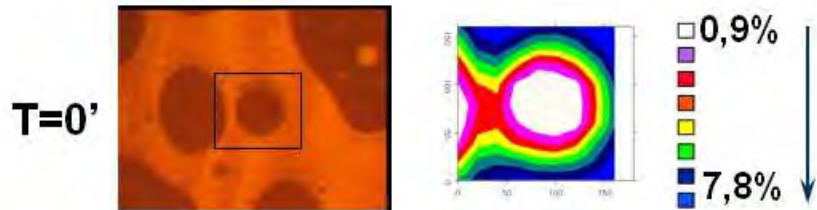
In situ Oxidation Analysis



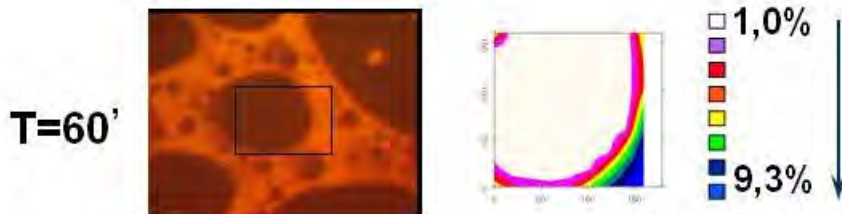
Oxidation cell to analyze in situ the aging effect on PMA structure

- Temperature sweep
- Heating rate
- Oxidant or neutral gas
- Allowing to continuously visualize and analyze the chemical evolution of phases

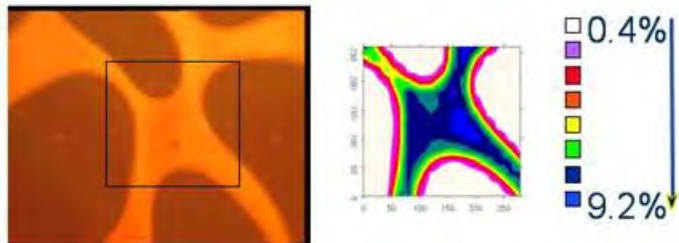
Effect of additives and aging on of Asphalt Structure



- Before aging



- After 60 min in aging cell 130°C/air
- Same focus



- After RTFOT+PAV aging

Aging effect on PMA structure by IR Microscopy

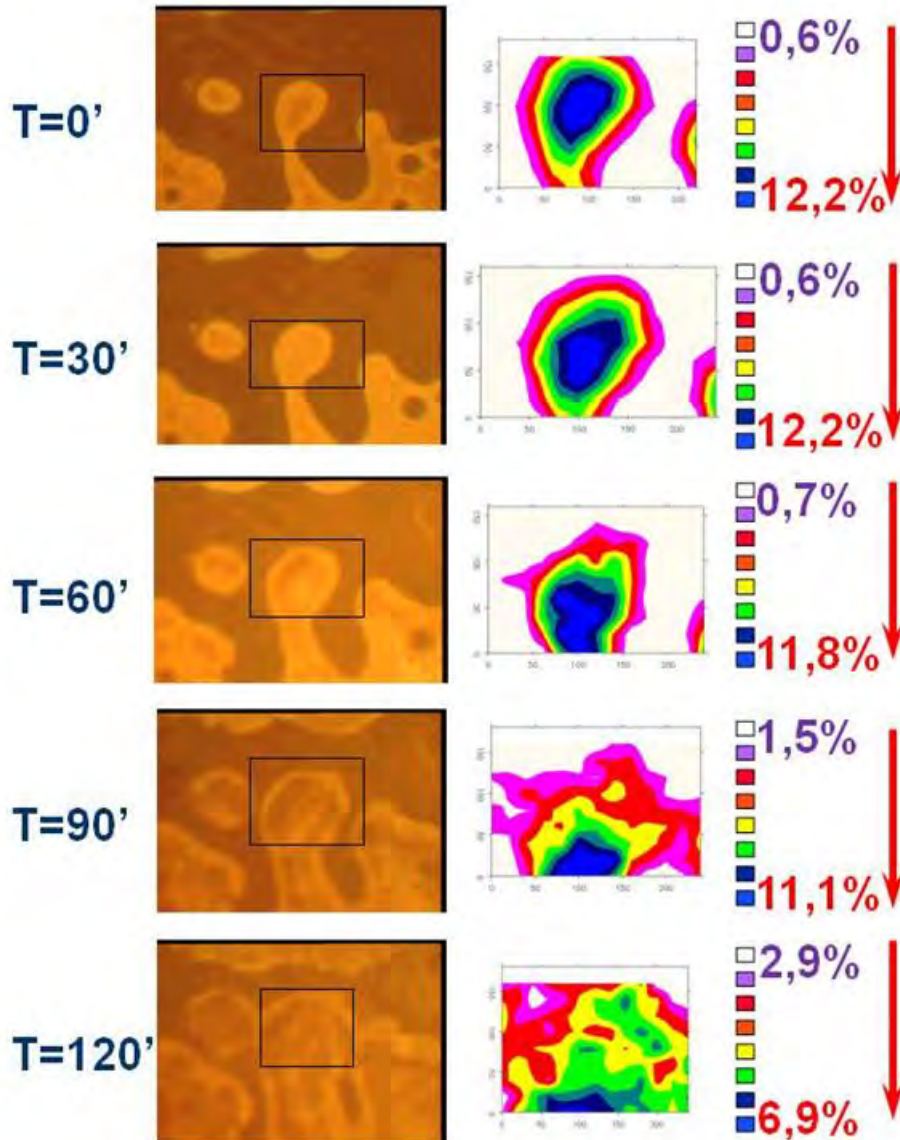
Before aging

- Phase inversion at 6% EVA
- EVA swollen by slightly condensed aromatics substituted by aliphatics

After aging

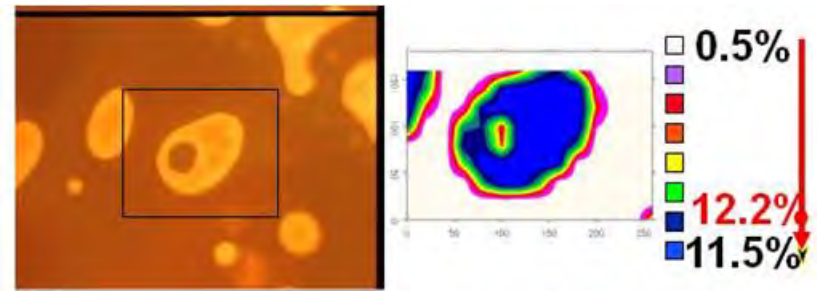
- % EVA increase in polymer nodules
 - Stability of aromatics and decrease in aliphatics & condensed aromatics
- migration of the fraction swelling EVA to the surrounding matrix

Effect of additives and aging on of Asphalt Structure

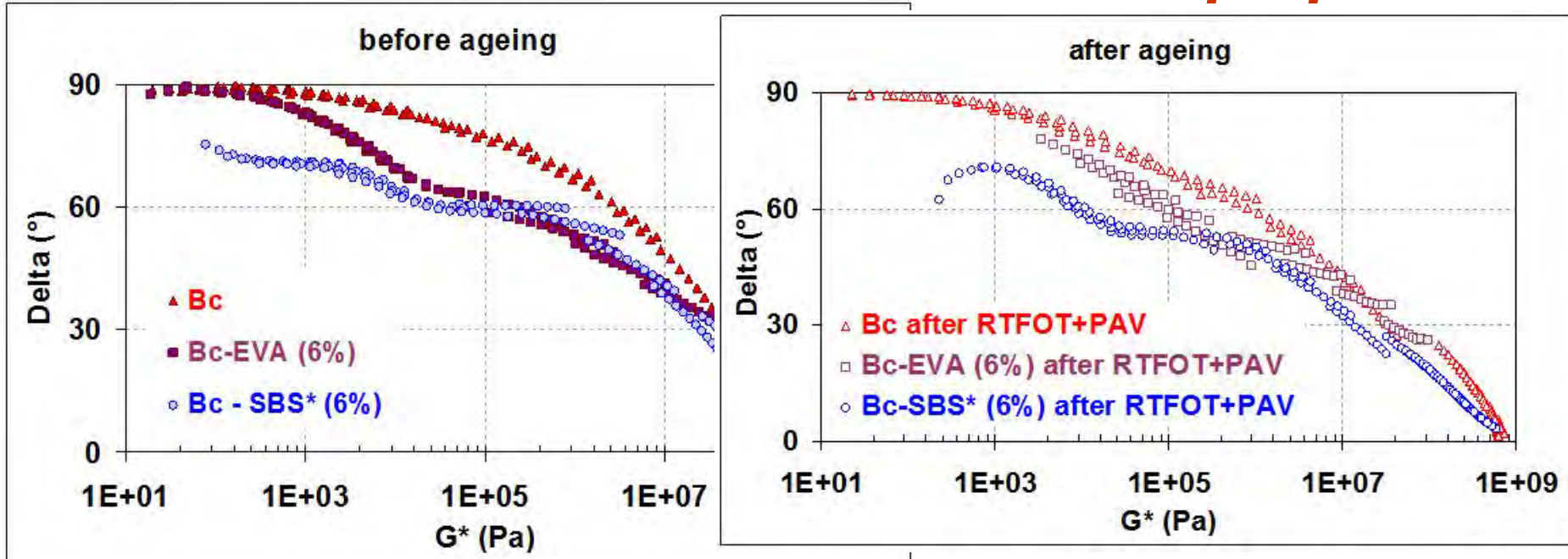


Ageing conditions : 130°C / Air

- ❑ PMB with 6% SBS linear
- ➔ Homogenization of SBS
 - ➔ Decrease in SBS content in polymer nodules
 - ➔ Increase in SBS in bitumen matrix
- ➔ Lower oxidation level (oxydes)
- ➔ In line with RTFOT+PAV

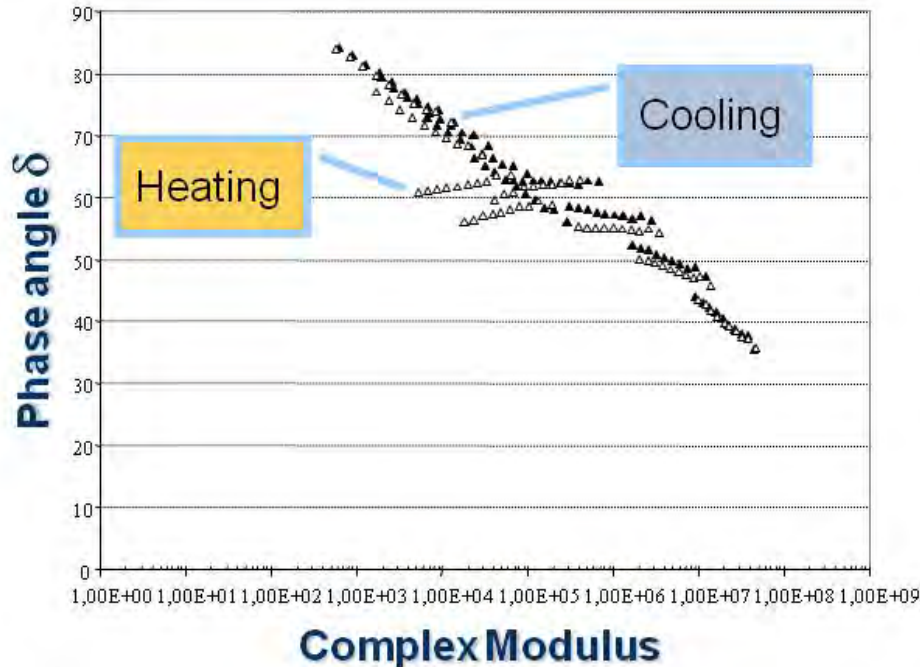


Effect of additives on Asphalt Mechanical properties



- Polymers impart a rubbery plateau effect – depending on polymer content, process
 - Confirmed by MSCR results outside the linear range
- Rubbery effect degrades upon oxidation – differently for SBS vs EVA
 - EVA itself is not oxidized, but its compatibility with oxidized asphalt molecules decreases
 - SBS oxidizes (chain scissions) but becomes more compatible

Effect of additives on Asphalt Mechanical properties

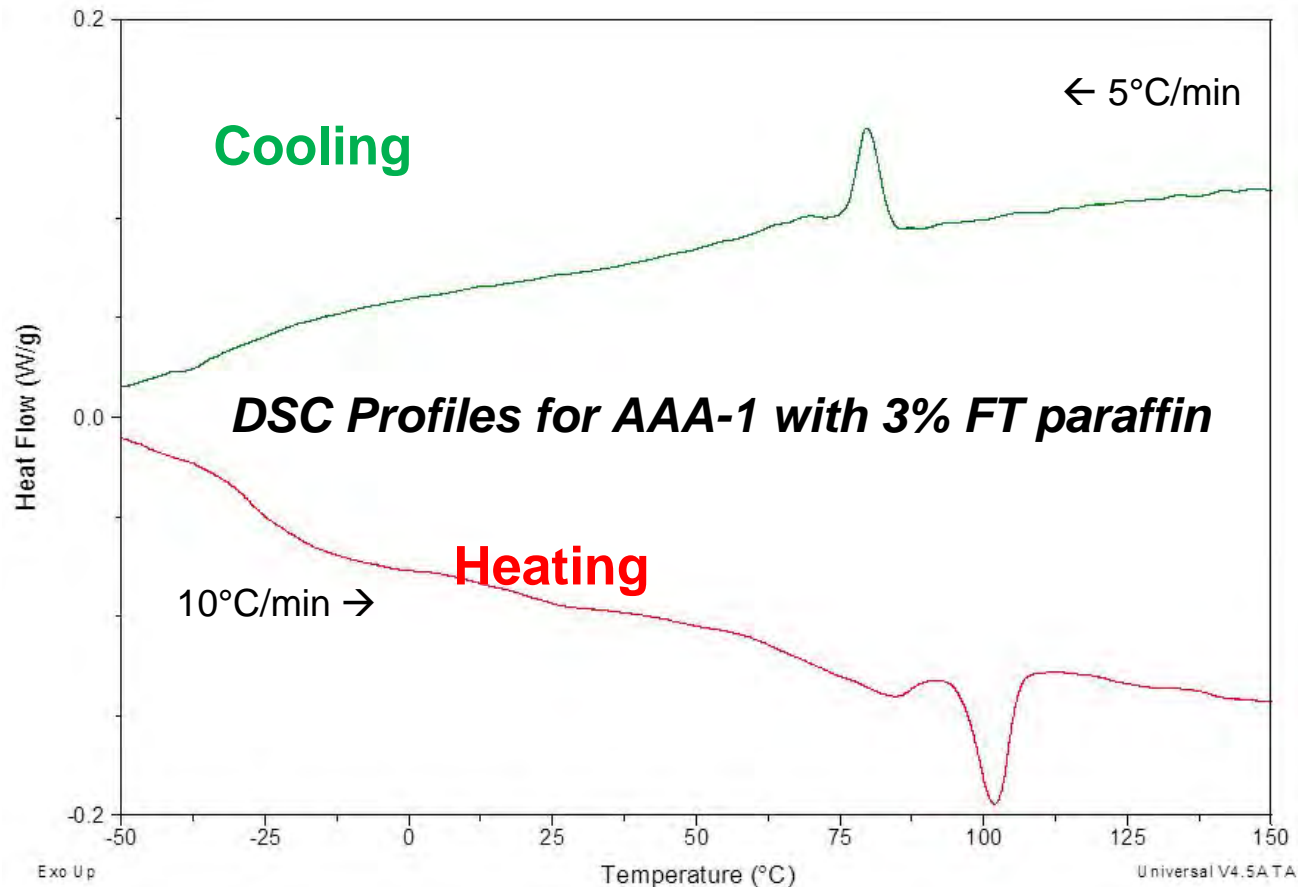


- **EVA crystallinity effect on binder properties (6% EVA):**
 - ✓ No single curve in Black space – TTSP not applicable
 - ✓ No rheological behavior superposition between cooling and heating

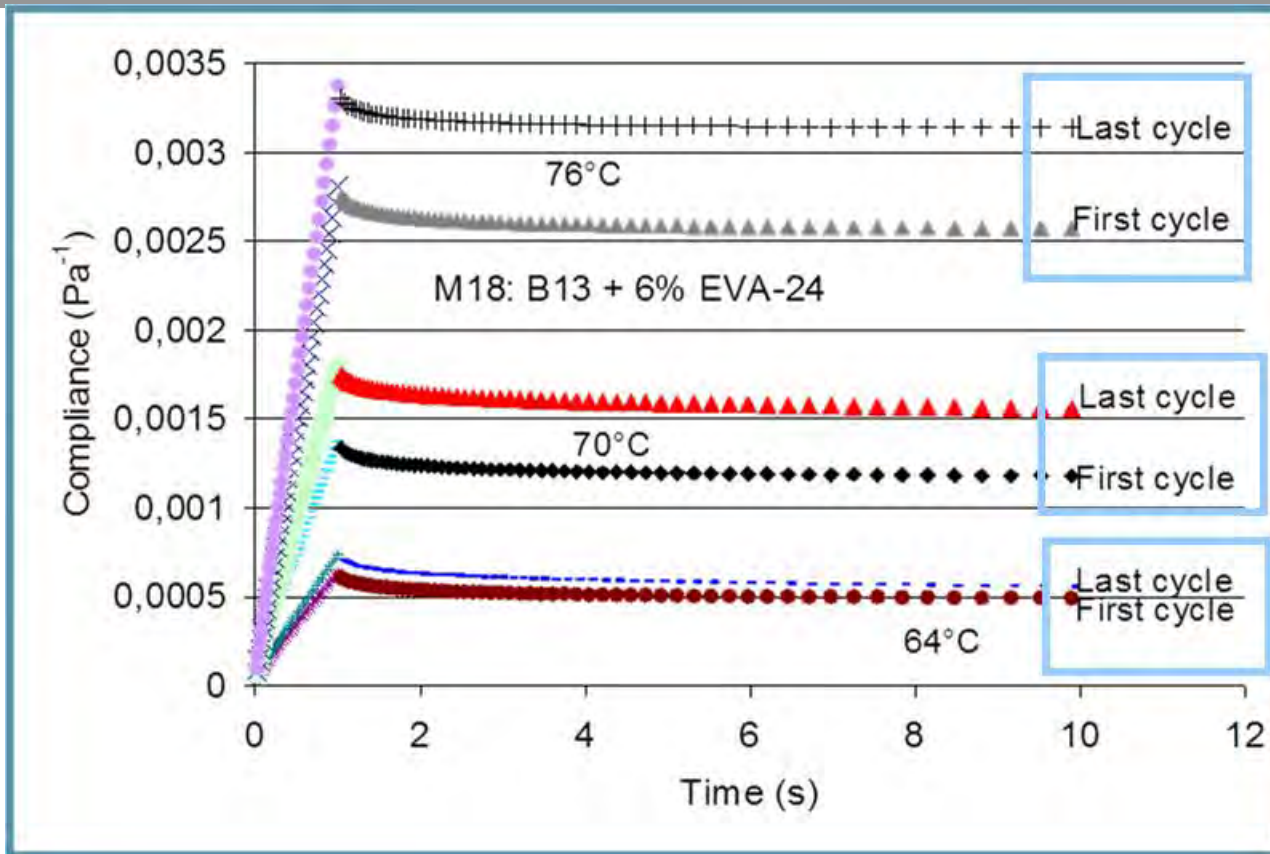
- **Dependency on crystallinity - Plastomer PMA**
 - Influence of thermal history on crystalline properties
 - Crystallization vs. Melting hysteresis in DSC - Cooling vs. Heating
 - Occurs with FT paraffins and PE type polymers
- **Works: Largeaud, Brule late 90's, Mouillet 2000's, WRI 2014**

Effect of additives on Asphalt Mechanical properties

Crystalline additive dependency on thermal history by
Differential Scanning Calorimetry – valid for PE, EVA, EBA,
FT Paraffin, amid wax...



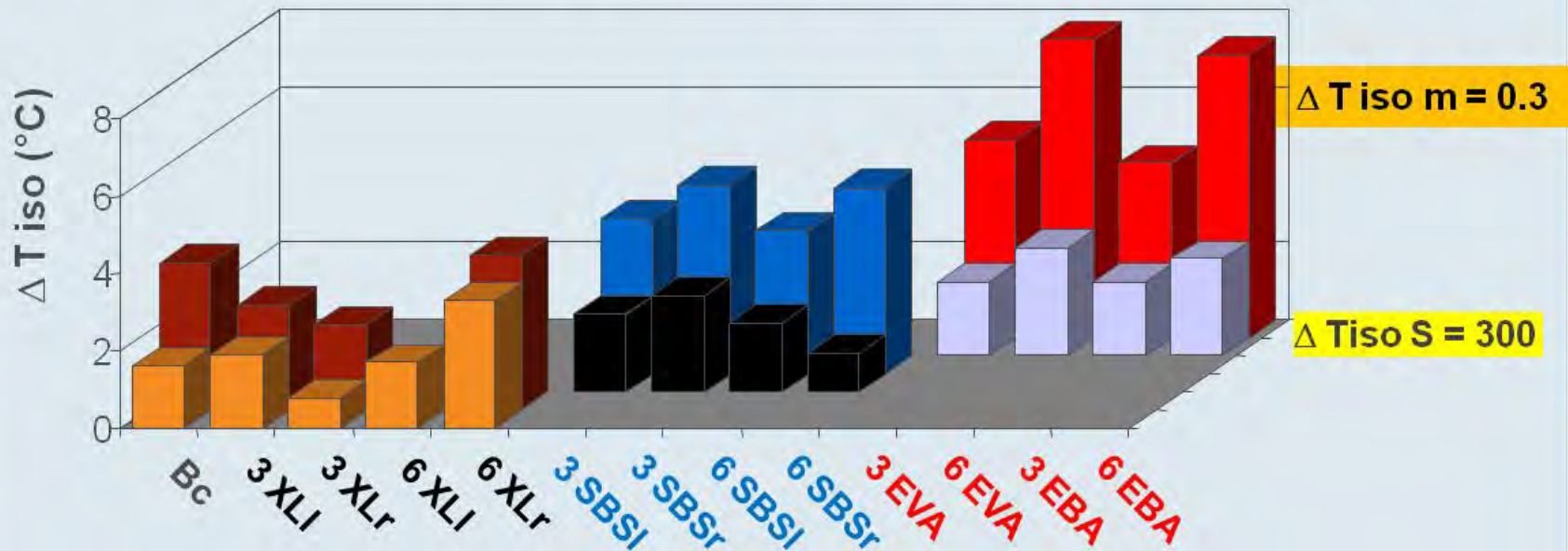
Effect of additives on Asphalt Mechanical properties



- **Repeated creep recovery test** for EVA PMA: softening effect
 - Modulus loss with time and T due to melting of PE crystalline fraction
 - No change in elastic recovery - ER very small for plastomers PMA
- **Works by Le Hir, Binard, Anderson, TRB 2001, E&E 2004**

Effect of additives on Asphalt Mechanical properties

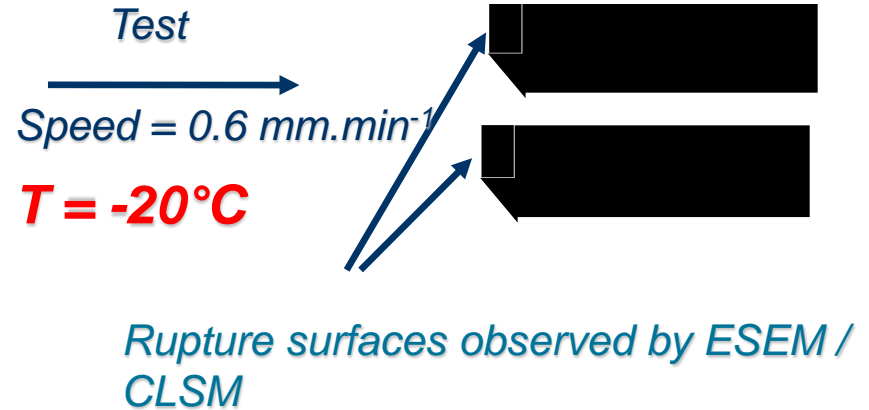
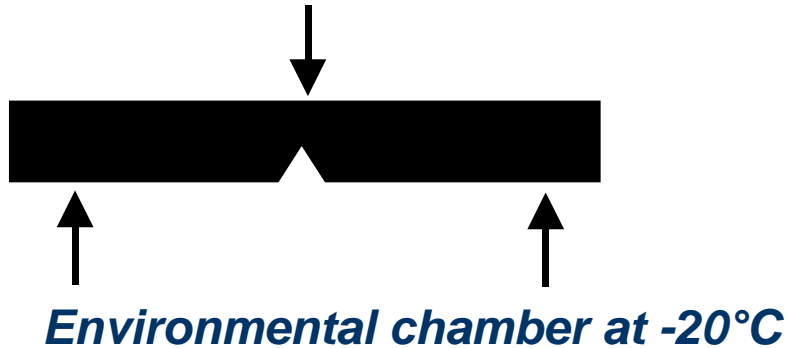
BBR parameters evolution: Unaged vs. RTFOT+PAV aged



- PMA's low temp properties (BBR) greatly affected by aging
 - M-value more "severe" indicator of binder aging
 - EVA PMA more affected than SBS, especially crosslinked which seem to resist oxidation better than the base
 - M-value relates to field cracking (EPFL – LAVOC study in CH)

Effect of additives on Asphalt Mechanical properties

Mode-I Fracture Test



- **Fracture mechanics** to assess low temperature fracture properties

- $K_{IC} = \text{failure load} \times f$ (span, crack length, sample dimensions)

- Observation by **ESEM/CLSM** – cold transfer

- Works by Hesp (CA), Lapalu et al (FR) - 2000

Neat asphalt

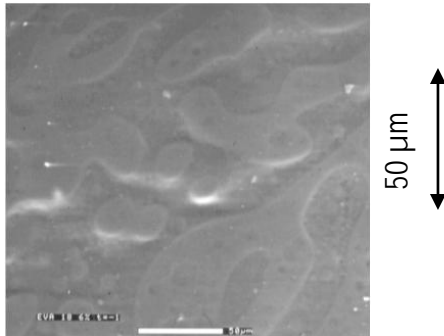
($K_{IC} = 48 \text{ kPa.m}^{1/2}$)



- No topographic contrast
- Brittle rupture \Rightarrow low K_{IC}

Effect of additives on Asphalt Mechanical properties

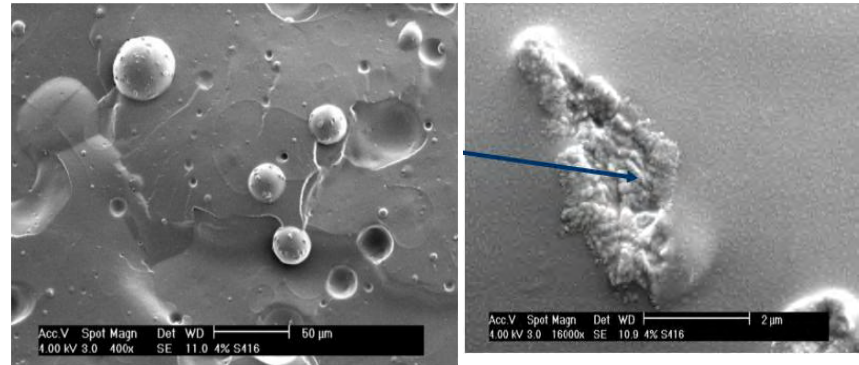
6% EVA-28 blend ESEM obs.
($K_{IC} = 74 \text{ kPa}\cdot\text{m}^{1/2}$) at -5°C



- Polymer glassy at test temperature
- Polymer-rich particles pulled-out with no deformation
- Fracture mechanism governed by the (poor) adhesion between phases
- \Rightarrow low K_{IC}

• Works by Lapalu et al (FR) - 2000

Physical blend 4% SBS* CLSM obs.
($K_{IC} = 107 \text{ kPa}\cdot\text{m}^{1/2}$) at -165°C



- Particle pull-out (crack deflection)
- Plastic deformation of SBS nodules
- SBS in rubbery state \Rightarrow High K_{IC}

4% Crosslinked SBS
($K_{IC} = 113 \text{ kPa}\cdot\text{m}^{1/2}$)



- **Background - Context**
- **Chemical-physical and structural properties of asphalt**
 - **Impact on asphalt mechanical properties**
- **Asphalt modification**
 - **Impact on structure and mechanical properties**
- **Summary**
- **Perspectives**



- **Asphalt binder physical properties are intimately related to their chemical composition and structure, with a very high dependency on the thermal history**
 - Associations – interactions - Wax precipitation - dissolution
 - Phases – multiple – exchanges – molecule transfer
 - Glass transition
 - Physical and chemical oxidative aging / hardening
- **Comparing binders in the same physical state to measure intrinsic properties is essential**
- **Asphalt modification incl. RAP drastically change structure, rheology, event the effect of aging**
 - Compatibility / Polymer swelling
 - Chemical reactions like binder oxidation, PMA crosslinking
- **“Real life” is impacted by those features**
 - Binder formulation and testing
 - Performance in the field

- ***Application of relevant material/chemical analyses to asphalt can make a change in understanding and designing asphalt materials***
- ***Some already did***
 - *Rheology-Mechanics: DSR, DMA, FT*
 - *Thermal analysis: DSC*
 - *Chromatography: TLC, HPLC, SEC-GPC*
 - *Microscopy techniques: IR, AFM, ESEM*
 - *Spectroscopy: IR*
- ***New characterization techniques will have impact on product development and vice versa: PMA, WMA...***
 - *Method coupling will become more affordable and usable*

Thank you !

